

Risk assessment and experimental design in the development of a prolonged release drug delivery system with paliperidone

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Abstract: This study focuses on the development of a drug product based on a risk assessment-based approach, within the quality by design paradigm. A prolonged release system was proposed for paliperidone (Pal) delivery, containing Kollidon® SR as an insoluble matrix agent and hydroxypropyl cellulose, hydroxypropyl methylcellulose (HPMC), or sodium carboxymethyl cellulose as a hydrophilic polymer. The experimental part was preceded by the identification of potential sources of variability through Ishikawa diagrams, and failure mode and effects analysis was used to deliver the critical process parameters that were further optimized by design of experiments. A D-optimal design was used to investigate the effects of Kollidon SR ratio (X_1), the type of hydrophilic polymer (X_2), and the percentage of hydrophilic polymer (X_3) on the percentages of dissolved Pal over 24 h (Y_1 – Y_9). Effects expressed as regression coefficients and response surfaces were generated, along with a design space for the preparation of a target formulation in an experimental area with low error risk. The optimal formulation contained 27.62% Kollidon SR and 8.73% HPMC and achieved the prolonged release of Pal, with low burst effect, at ratios that were very close to the ones predicted by the model. Thus, the parameters with the highest impact on the final product quality were studied, and safe ranges were established for their variations. Finally, a risk mitigation and control strategy was proposed to assure the quality of the system, by constant process monitoring.

Keywords: pharmaceutical development, quality by design, failure mode effects analysis, Ishikawa diagram, fish-bone diagram, hydrophilic matrix

Introduction

Pharmaceutical product preparation includes complex material (active principles and excipients) processing, consisting of numerous independent or continuous stages.¹ Each operation comes with its own sources of variability. Novel concepts, taken up by the regulatory agencies, require the “built-in” quality of a drug product, through a scientifically proven, quality by design approach, which is meant to predict and control all sources of errors.^{2–4}

From the development stage of a new formulation, a complete quality target product profile (QTPP) should be established, with the desired characteristics of the product and the critical quality attributes (CQAs) that have to be monitored in the intermediate and final stages of the preparation procedure.⁵ Risk assessment analysis involves one or more of the following tools: Ishikawa diagrams, failure mode effects analysis (FMEA), and hazard analysis and critical control points (HACCPs), and it is supposed to identify and rank the critical process parameters (CPPs).⁶ Usually, the variables that have an impact on CQAs are interconnected; therefore, their study using design of experiments (DoEs)

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was useful to assess and predict both their individual and interacting effects. Statistical calculations of the multifactorial relationships with the use of response surface methodology lead to the development of a design space, meaning a domain of input variables, which guarantee the delivery of a product with the required characteristics.^{5,7}

A prolonged release drug delivery system requests rigorously controlled dissolution kinetics and the thorough understanding of the variables that could influence the system, so that it could be predicted quantitatively with a high precision.^{8,9} Polymeric matrix systems were extensively studied due to their simple preparation by direct compression and their easily available excipients. Hydrophilic polymers such as hydroxypropyl methylcellulose (HPMC), hydroxypropyl cellulose (HPC), and sodium carboxymethyl cellulose (CMCS) were used in the formulation of controlled release matrices, individually or as mixtures, and the drug transport kinetics depended on polymer hydration, swelling, and further erosion, as well as on drug dissolution and diffusion through the formed gel.^{10,11} On the other hand, insoluble matrices formed with hydrophobic polymers such as ethyl cellulose, Eudragit® RS (Evonik, Essen, Germany), or Kollidon® SR (BASF, Ludwigshafen, Germany) form porous structures upon hydration, and the dissolved active principle diffuses slowly through the pores into the liquid media.^{12–14}

Kollidon SR is a physical mixture of polyvinyl acetate and polyvinylpyrrolidone (PVP; 8:2) prepared by direct compression, widely used for extended-release matrix tablets.¹³ They keep intact shape and dimensions passing through the gastric tract and facilitate the transport of the drug through the pores formed by PVP dissolution, in a diffusion-controlled manner. From the previous studies, it was found that water uptake rates in Kollidon SR matrices were very high at first media exposure, and then, they settled to a constant level when the matrix was completely soaked.¹⁵ Therefore, parameters such as pore sizes, Kollidon SR content, and matrix density principally regulate the release.

Paliperidone (Pal) was approved for schizophrenia treatment as an atypical antipsychotic and is available as Invega® prolonged release tablets that contain from 1.5 to 12 mg active principle. It is a weak base and practically insoluble in water,¹⁶ especially at increasing pH,¹⁷ and the absolute oral bioavailability is of only 28%.¹⁸ Controlled drug release techniques could assure a convenient dosing frequency and a steady-state drug level, which are beneficial for the patient's comfort.

The present research work aimed at developing a prolonged release matrix tablet with Pal, within the concept of

quality by design. The drug was included in an inert matrix made of Kollidon SR, to which hydrophilic polymers were added; a drug delivery system that, to the authors' knowledge, had not been explored enough. The authors intended to modulate the release kinetics by a combined mechanism: one limitation imposed by the porous structure generated with the insoluble polymer and the other from the hydrophilic polymer gelling and slow drug diffusion.

Materials and methods

Materials

The following active principle and excipients were used: Pal (Apotex Pharmachem, Bangalore, India), lactose (FlowLac® 100; Meggle, Wasserburg am Inn, Germany), physical mixture of polyvinyl acetate and povidone (8:2) – Kollidon RS, HPC, (LH21; Shin-Etsu, Tokyo, Japan), HPMC (METHOCEL™ K4M Premium CR; Colorcon, Dartford, UK), CMCS (Fluka Chemie GmbH, Buchs, Switzerland), silicon dioxide, (Aerosil®; Evonik), and magnesium stearate (Union Derivan, Barcelona, Spain).

Tablet preparation

Pal was mixed with the compression excipients by means of geometric dilution, following the compression formulas, presented in the tables, in the preliminary part of the study and the experimental design. Tablets were manufactured by using an eccentric tablet press (Korsch EK0; Korsch, Berlin, Germany) equipped with a series of different diameter set punches (as shown in the descriptions of tablet formulas). The tablet press was adjusted for a fixed tablet weight that corresponded to a content of 3 mg Pal/tablet.

Tablet pharmaceutical characterization

Tablets were characterized for crushing strength (Dr Schleuniger, Radevormwald, Germany) and for Pal release at different times over 24 h (0.5, 1, 2, 4, 6, 8, 12, 18, and 24 h). The percentage of dissolved Pal was assessed by the European Pharmacopoeia method, by using a Pharma Test PT-DT7 system, apparatus no 1 (basket), at 37°C±0.5°C, 100 rpm, in 900 mL phosphate buffer (pH=6.8); 5 mL samples were redrawn at every specified time and replaced with the same volume of fresh media. The drug assay was performed by high-performance liquid chromatography/ultraviolet method (HPLC Agilent 1100; equipped with a Gemini C18 110 Å 50×3 mm ×5 µm column), having acetonitrile/0.1% phosphoric acid aqueous solution (15:85) as a mobile phase, at a flow rate of 1 mL/min. Pal was detected at 277 nm, at a retention time of 1.17 min.

For the release kinetics evaluation, the results were fitted with several mathematical equations: Baker and Lonsdale, Peppas, Hixon and Crowell, Higuchi, first order, and zero order.

Identification of the QTPP, CQAs, and risk analysis of CQAs

According to International Conference on Harmonisation (ICH) Q8, QTPP contains a set of characteristics of the pharmaceutical product, which are related to its quality, safety, and efficacy.⁵ Table 1 lists the QTPP for the extended-release Pal tablets, and the identified product quality features represent the basis for CQA defining. For each of the CQAs, an Ishikawa diagram was developed, as a risk assessment tool used to identify potential variables that could have an impact on the particular quality attribute.¹⁹

Risk assessment by FMEA

An overall risk evaluation is depicted in the Ishikawa diagrams that contain all the process parameters that can influence or produce a failure concerning the quality of the final product. FMEA method allows the identification and prioritization of the failure modes that are most likely to cause product failure. The prioritization follows three criteria: frequency of occurrence, stringency of effects, and difficulty of detection. Each of these attributes was evaluated on a scale from 1 to 5, as follows: the occurrence (O) was ranked as 5 for frequent, 4 for probable, 3 for occasional, 2 for remote, and 1 for improbable; the severity (S), meaning the consequences of the failure mode, was classified as 5 for catastrophic, 4 for critical, 3 for serious, 2 for minor, and 1 for negligible; finally, the third criterion, the detectability (D), meaning the difficulty to identify the failure mode, was ranked as 5 for hard to detect, 4 for low chance to be detected, 3 for moderately detectable, 2 for highly detectable, and 1 for easily detectable. The three attributes were evaluated for each of the considered CPPs. The failure risk was calculated as risk priority number (RPN) = O×S×D (Table 2).^{20,21}

The highest ranked CPPs were explored in the preliminary experiments and the further experimental design.

Preliminary experiments

The preliminary experimental part aimed at establishing convenient size, weight, and mechanical strength for the Pal tablets in order to ensure appropriate weight uniformity, hardness, and dissolution profiles.

First, four formulations were prepared according to the data presented in Table 3, with increasing medium weights and sizes and the same hardness. Their dissolution profiles were evaluated, and consequently, final weight and size were selected for further experiments. Next, five formulations were prepared, by using the same qualitative and quantitative composition, but processed with increasing compression forces. Subsequently, the effect of the compression force on Pal release was determined, and an optimal compression force was chosen for the rest of the trials.

Design of experiments

A D-optimal DoE was chosen, due to the precise estimation of factor effects and the low number of experimental trials compared with standard factorial design. Based on the Ishikawa diagrams, three key variables were identified that could influence the Pal release, apart from the size, weight, and mechanical strength that were already set to optimal values. The DoE was developed by using Modde 11.1 software (Umetrics, Umea, Sweden), and it comprised 18 runs and three center points, therefore 21 experiments, as shown in Table 4. Each of the formulations contained Kol-lidon SR as an inert matrix-forming agent in one of the four concentrations 25%, 30%, 35%, or 40% and 0%, 5%, or 10% of one of the chosen hydrophilic polymers (HPC, HPMC, or CMCS). As for the responses, the Pal release at each of the nine sampling times (Y_1 – Y_9) was included in the DoE, as well as the k and n coefficients in Peppas kinetic equation (Y_{10} and Y_{11}). The responses were expressed mathematically

Table 1 QTPP of paliperidone extended-release tablets

QTPP element	Target	Observations
Route of administration	Oral	
Dosage form	Extended-release tablet	
Dosage strength	3 mg	
Drug product quality attributes	Physical properties	No defects, meaning no chipping, lamination, or capping Meeting compendia claims, between 90% and 110% of the declared paliperidone
	Assay	
	Dissolution	24-h extended release
Container closure system	Suitable for storage in normal conditions	Ensures product integrity during shelf life

Abbreviation: QTPP, quality target product profile.

Table 2 Failure mode effects analysis for risk assessment

CPP	Failure mode	Failure effects	Potential causes	Control methods	O	S	D	RPN
Punch and die size	Unsuitable punch and die size	Weight uniformity, hardness, friability, Pal release	Unsuitable punch and die size	Diameter and height measuring	1	5	2	10
Compression force	Improper compression force	Hardness, friability, Pal release	Machine error, human error, different excipients	Hardness test, dissolution test	2	5	3	30
Kollidon® SR ratio	Unsuitable concentration	Pal release	Unsuitable concentration, different excipients	Dissolution test	5	5	3	75
Hydrophilic polymer ratio	Unsuitable concentration	Pal release	Unsuitable concentration, different excipients	Dissolution test	5	5	3	75
Hydrophilic polymer type	Inappropriate type	Pal release	Inappropriate type	Dissolution test	1	5	3	15

Abbreviations: CPP, critical process parameter; D, detectability; O, occurrence; RPN, risk priority number; S, severity; Pal, paliperidone.

as equations that describe their relation to the formulation variables:

$$Y = b_0 + b_1X_1 + b_2X_2 + b_3X_3 + b_4X_1^2 + b_5X_2^2 + b_6X_3^2 + b_7X_1X_2 + b_8X_2X_3 + b_9X_1X_3 + b_{10}X_1X_2X_3 \quad (1)$$

where Y is the response, b_0 is the mean value of the response, and b_i are regression coefficients. The regression coefficients indicate the direction and the magnitude of the effect. X_1 , X_2 , and X_3 are individual effects that are results of variation in one factor, whereas all the other factors are kept at constant values. X_1^2 , X_2^2 , and X_3^2 are second-order terms that can reveal the curvatures in the effects' variations. X_1X_2 , X_2X_3 , X_1X_3 , and $X_1X_2X_3$ are interaction effects that show the variation of the responses when two or more factors changed simultaneously.

The generated models were improved by backward elimination of the insignificant terms and the revised values of the regression coefficients, together with their statistical significance expressed as P -values (significant when $P < 0.05$), which are listed in Table 5. The positive or negative value of the regression coefficient represents the positive or the negative influence the effects have on the response.

Table 5 lists the results of the analysis of variance (ANOVA). The quality of model fit was assessed by

Table 3 Qualitative and quantitative composition of tablets used for the evaluation of tablet weight influence on the paliperidone release

	FI (%)	FII (%)	FIII (%)	FIV (%)
Paliperidone	2.5	2	1.2	0.833
Lactose	56.75	57.25	58.05	58.416
Kollidon® SR	40	40	40	40
Silicon dioxide	0.5	0.5	0.5	0.5
Magnesium stearate	0.25	0.25	0.25	0.25
Tablet weight (mg)	120	150	250	360
Tablet diameter (mm)	6	7	8	10
Tablet surface (mm ²)	120.5	152.3	200.9	269.1

Note: FI, FII, FIII, and FIV are preliminary tablet formulations.

calculating the regression coefficient (R^2) between the observed and the predicted responses.²²

In order to complete the statistical analysis, three-dimensional response surfaces were generated according to the revised regression equations (Table 6). The DoE comprised two quantitative factors (X_1 , Kollidon SR percentage; and X_3 , hydrophilic polymer percentage) and one qualitative factor (X_2 , the type of hydrophilic polymer: HPC, HPMC, or CMCS); therefore, the surfaces were graphical representations of the response as a function of X_1 and X_3 , whereas X_2 was consecutively HPC, HPMC, and CMCS.

Results and discussion

QTPP and CQAs of Pal prolonged release tablets

The QTPP of each pharmaceutical product was established according to the type of dosage form and preparation process. Based on preliminary studies, literature data, and researchers' experience, the QTPP elements and their associated targets were framed as in Table 1.

The CQAs that were derived from the previously developed QTPP were crushing strength, the weight uniformity, and the in vitro dissolution profile. In order to have a clear image on the preparation process and to be able to thoroughly control and prevent any minor error, an Ishikawa diagram was developed for each of the CQAs (Figure 1). The CPPs were listed and evaluated by FMEA method, and the parameters with the highest RPN were considered for optimization through preliminary studies and DoE. The significance of the RPN values was highly risky for $RPN \geq 40$, medium risk for $RPN \geq 20$ and $RPN < 40$, and low risk for $RPN < 20$.²¹

The punch and die size, the compression force, and the insoluble and soluble polymers as formulation factors were present as failure modes with high RPNs (Table 2) in the FMEA. The highest risk was met by the formulation parameters, Kollidon SR ratio and hydrophilic polymer

Table 4 Design matrix and results

Exp	X ₁ (%)	X ₂	X ₃ (%)	X ₄ (kN)	Response		Y ₁ (%)	Y ₂ (%)	Y ₃ (%)	Y ₄ (%)	Y ₅ (%)	Y ₆ (%)	Y ₇ (%)	Y ₈ (%)	Y ₉ (%)
N1	25	HPC	0	202.3	35.64±1.24	51.23±1.44	65.6±1.56	82.47±0.73	93.8±4.05	95.77±4.38	93.77±4.38	95.77±4.38	93.77±4.38	92.9±6.05	92.44±5.78
N2	25	HPC	10	195.6	34.6±3.73	53.04±5.00	73.72±4.66	86.9±11.83	93.2±8.78	95.58±6.23	99.88±1.08	95.58±6.23	99.88±1.08	98.22±0.73	97.88±2.18
N3	25	HPC	5	220.3	17.81±0.68	29.63±1.25	46.43±7.94	64.82±15.83	74.88±15.98	81.28±1.4	90.59±8.98	81.28±1.4	90.59±8.98	94.46±2.84	95.76±0.85
N4	30	HPC	0	220.2	9.06±0.19	13.58±0.81	19.21±1.35	27.5±1.13	32.98±0.33	40.01±1.05	48.11±1.35	40.01±1.05	48.11±1.35	57.52±0.78	65.61±1.69
N5	35	HPC	10	228.8	13.01±0.91	19.48±0.75	28.26±2.44	46.74±6.84	59.42±10.22	67.79±12.16	80.53±14.23	67.79±12.16	80.53±14.23	92.03±15.31	94.68±12.81
N6	40	HPC	0	281.8	7.39±0.47	10.44±0.62	14.47±0.99	20.09±1.53	24.69±1.42	28.93±1.45	35.47±1.44	28.93±1.45	35.47±1.44	45.86±2.51	51.12±2.64
N7	40	HPC	10	260.4	11.31±2.03	19.34±1.62	27.56±2.74	36.71±3.49	43.72±5.06	49.18±5.87	58.38±6.59	49.18±5.87	58.38±6.59	67.22±8.32	72.52±8.94
N8	40	HPC	5	215.5	7.99±0.16	11.27±0.31	15.7±0.64	22.54±0.93	27.17±1.72	30.5±2.19	37.43±2.56	30.5±2.19	37.43±2.56	45.7±3.54	51.44±4.47
N9	25	HPMC	0	202.3	35.64±1.24	51.23±1.44	65.6±1.56	82.47±0.73	93.8±4.05	95.77±4.38	93.77±4.38	95.77±4.38	93.77±4.38	92.9±6.05	92.44±5.78
N10	25	HPMC	10	202.8	7.5±1.59	15.19±2.12	24.65±1.31	40.13±0.88	53.33±0.95	63.3±0.86	78.39±2.71	63.3±0.86	78.39±2.71	89.44±1.17	92.58±0.81
N11	30	HPMC	5	242.7	6.98±0.38	11.46±0.84	20.41±0.83	30.2±0.25	37.92±1.41	43.18±2.18	52.36±2.89	43.18±2.18	52.36±2.89	61.19±3.35	67.74±2.74
N12	40	HPMC	0	281.8	7.39±0.47	10.44±0.62	14.47±0.99	20.09±1.53	24.69±1.42	28.93±1.45	35.47±1.44	28.93±1.45	35.47±1.44	45.86±2.51	51.12±2.64
N13	40	HPMC	10	209.4	5.57±0.20	9.79±0.20	15.67±0.14	24.62±0.3	30.88±0.65	37.8±0.35	45.76±0.5	37.8±0.35	45.76±0.5	54.57±0.14	61.16±0.04
N14	25	CMCS	0	202.3	35.64±1.24	51.23±1.44	65.6±1.56	82.47±0.73	93.8±4.05	95.77±4.38	93.77±4.38	95.77±4.38	93.77±4.38	92.9±6.05	92.44±5.78
N15	25	CMCS	10	209.8	8.14±0.44	13.88±1.65	23.62±0.79	35.44±0.15	42.18±0.36	46.87±0.51	54.49±1.28	46.87±0.51	54.49±1.28	62.58±1.66	68.14±2
N16	35	CMCS	5	196.6	6.75±0.06	10.5±0.20	15.58±0.39	22.82±0.53	27.11±0.04	33±0.08	40.21±0.52	33±0.08	40.21±0.52	47±0.83	52.38±0.05
N17	40	CMCS	0	281.8	7.39±0.47	10.44±0.62	14.47±0.99	20.09±1.53	24.69±1.42	28.93±1.45	35.47±1.44	28.93±1.45	35.47±1.44	45.86±2.51	51.12±2.64
N18	40	CMCS	10	194.1	6.85±0.45	10.27±0.28	15.15±0.37	22.29±1.02	27.62±1.41	31.67±1.59	39.1±2.35	31.67±1.59	39.1±2.35	48.4±0.53	53.55±0.48
N19	35	CMCS	5	226.5	10.24±1.48	15.41±1.73	20.39±1.99	27.53±3.01	32.76±2.23	37.53±2.46	43.96±1.82	37.53±2.46	43.96±1.82	52.76±0.89	59.06±3.29
N20	35	CMCS	5	255.3	6.87±0.97	10.4±0.87	15.85±0.76	23.17±0.96	28.37±0.76	32.14±1.02	38.81±1.62	32.14±1.02	38.81±1.62	45.95±1.68	52.07±1.58
N21	35	CMCS	5	241.4	6.47±0.43	10.19±0.59	15.17±0.70	22.37±0.52	28.11±0.72	32.21±0.82	39.88±1.12	32.21±0.82	39.88±1.12	47.03±1.47	53.63±1.93
Target values					5	15	25	35	45	55	65	55	65	75	85
Optimal formulation experimental values					6.57±0.35	12.23±0.84	21.35±1.20	34.5±1.23	43.94±0.45	53.1±0.64	65.1±1.33	53.1±0.64	65.1±1.33	75.12±1.33	82.81±1.08
Optimal formulation predicted values					5.00	10.42	19.14	34.32	44.17	52.71	65.20	52.71	65.20	74.89	82.52
Residual					1.57	1.81	2.21	0.18	-0.23	0.39	-0.10	0.39	-0.10	0.23	0.29

Notes: X₁, Kollidon® SR percentage; X₂, type of hydrophilic polymer; X₃, hydrophilic polymer percentage; X₄, hardness (kN), controlled variable; Y₁–Y₉, percentage of released paliperidone after 0.5, 1, 2, 4, 6, 8, 12, 18, and 24 h. Pal release was reported as mean dissolved percentage ± standard deviation of tested tablets.

Abbreviations: CMCS, sodium carboxymethyl cellulose; HPC, hydroxypropyl cellulose; HPMC, hydroxypropyl methylcellulose; Pal, paliperidone; Exp, experiment.

Table 5 Statistical parameters – analysis of variance test

Response	SS	MS	DF	F-value	P	R ²	Adjusted R ²	Q ²
Y ₁	5,223.42	261.17	19	15.80	0.000	0.920	0.862	0.735
Y ₂	11,460.80	573.04	19	18.77	0.000	0.932	0.882	0.775
Y ₃	21,064.70	1,053.23	19	24.86	0.000	0.948	0.909	0.826
Y ₄	45,361.90	2,160.09	20	16.98	0.000	0.919	0.865	0.715
Y ₅	60,966.20	2,903.15	20	18.79	0.000	0.926	0.877	0.755
Y ₆	70,381.70	3,351.51	20	20.20	0.000	0.931	0.885	0.776
Y ₇	84,068.70	4,003.27	20	21.37	0.000	0.934	0.891	0.891
Y ₈	99,451.90	4,735.80	20	15.79	0.000	0.913	0.855	0.717
Y ₉	109,630.00	5,220.48	20	18.01	0.000	0.907	0.856	0.757
Y ₁₀	34.29	1.63	20	23.44	0.000	0.939	0.899	0.723
Y ₁₁	2.26	0.11	19	6.28	0.003	0.820	0.690	0.391

Notes: Y₁–Y₉, percentage of released paliperidone after 0.5, 1, 2, 4, 6, 8, 12, 18, and 24 h. Y₁₀, k-Peppas. Y₁₁, n-Peppas.

Abbreviations: Adjusted R², adjusted value of the coefficient of determination; DF, degrees of freedom; F-value, Fischer's ratio; MS, mean of square; Q², predictive power of the model; p, probability; R², coefficient of determination; SS, sum of squares.

ratio, which could occur with improper mixing or excipient supplier changing. Compression force was considered as a medium-risk CPP that could arise due to equipment malfunction, human errors, or variations in excipient characteristics. Once set, the last two CPPs, punch and die size and the type of hydrophilic polymers, have low influence on product CQAs and, therefore, low RPNs.

The risk analysis resulted in dividing the experimental work into two parts, preliminary experiments for the empirical optimization of tablet diameter (punch and die size) and compression force, and further thorough study of the high-risk CPPs by DoE.

Preliminary experiments

First, the study aimed at exploring the influence of the tablet weight and surface on the aforementioned CQAs.

All formulations were within limits (relative standard deviation ≤5%) with respect to the weight uniformity test. In order to avoid double variable effect, the compression force was set so that the mechanical strength was constant. As shown in Figure 2A and B, Pal release increased with the tablet weight up to a value of 250 mg, due to the higher contact surface between the tablet and the dissolution media and the higher porosity created by the lactose and PVP dissolution,¹² but when surpassing this value, no further changes were noticed in drug dissolution.

As slow Pal dissolution was the most important prerequisite for this drug delivery system, the tablet preparation was continued by using punch and die with a diameter of 7 mm, in order to obtain tablets of 120 mg and 120 mm² average surface. This way, slow release is favored starting with the shape and the size of the tablet.

Table 6 Regression equation coefficients

Effect	Response								
	Y ₁	Y ₂	Y ₃	Y ₄	Y ₅	Y ₆	Y ₇	Y ₈	Y ₉
Constant	7.697	12.147	18.699	29.165	36.368	42.638	51.947	60.900	70.764
X ₁	-6.801	-10.525	-14.628	-21.327	-23.551	-23.322	-21.913	-18.630	-16.766
X ₂ (HPC)	0.825	1.469	2.441	6.338	6.456	6.583	7.126	6.738	6.545
X ₂ (HPMC)	-1.365	-1.820	-2.193	-4.014	-3.109	-2.153	-1.080	0.143	1.125
X ₂ (CMCS)	0.540	0.350	-0.248	-2.324	-3.346	-4.429	-6.045	-6.881	-7.671
X ₃	-5.321	-6.432	-6.431	-3.858	-3.549	-2.291	0.829	2.211	2.752
X ₁ ²	7.092	10.450	12.988	15.723	16.169	14.298	10.730	7.913	—
X ₂ ²	—	—	—	—	—	—	—	—	—
X ₃ ²	—	—	—	—	—	—	—	—	—
X ₁ X ₂	—	—	—	—	—	—	—	—	—
X ₁ X ₃	6.508	8.912	10.206	8.852	9.973	9.448	7.206	5.337	4.457
X ₂ (HPC) X ₃	3.856	5.686	7.399	12.943	13.644	12.856	11.844	10.056	8.428
X ₂ (HPMC) X ₃	-2.168	-2.739	-3.506	-5.594	-5.020	-3.608	-2.102	-0.899	-0.207
X ₂ (CMCS) X ₃	-1.688	-2.947	-3.893	-7.349	-8.623	-9.248	-9.742	-9.156	-8.220
X ₁ X ₂ X ₃	—	—	—	—	—	—	—	—	—

Notes: X₁, Kollidon® SR percentage; X₂, type of hydrophilic polymer; X₃, hydrophilic polymer percentage; Y₁–Y₉, percentage of released paliperidone after 0.5, 1, 2, 4, 6, 8, 12, 18, and 24 h. Bold values indicate statistical significance, with P<0.05.

Abbreviations: CMCS, sodium carboxymethyl cellulose; HPC, hydroxypropyl cellulose; HPMC, hydroxypropyl methylcellulose.

The impact of the compression force on the crushing strength was extensively studied; in the present case it produced an increase in the crushing strength from 57.5 ± 9.86 N to 384.5 ± 20.48 N. In order to assess the influence of the compression force on the Pal release, dissolution tests were conducted on formulations with the same content (FI tablets, Table 3), but with increasing crushing strength. As expected, the higher the crushing strength, the slower the release, but it seems that if an average value of 350 N is attained, the influence of the crushing strength weakens, up to a limit where

the dissolution profile is no longer affected (Figure 2B). In insoluble matrix-type tablets, drug release increases with the increase in initial porosity.²³ Lactose, the water-soluble filler, quickly dissolves in the media, leaving the water-filled pores that easily allow Pal release by diffusion. The diffusion coefficient was reported to rise with higher initial porosity, which explains the result obtained for the dissolution profiles.^{13,23}

Considering the obtained results, the compression force for the further formulations was set to obtain crushing strengths between 200 N and 300 N.

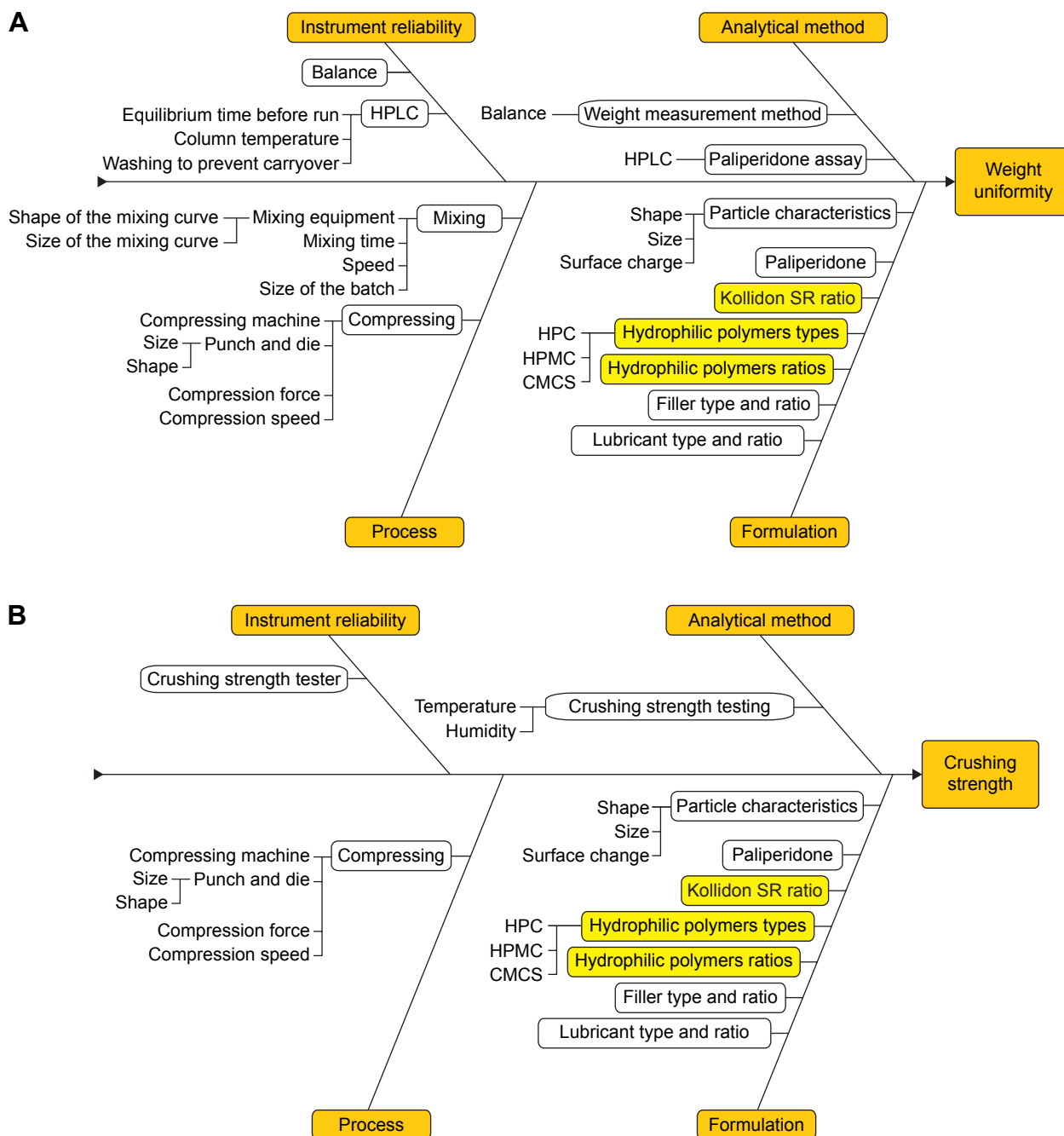


Figure 1 (Continued)

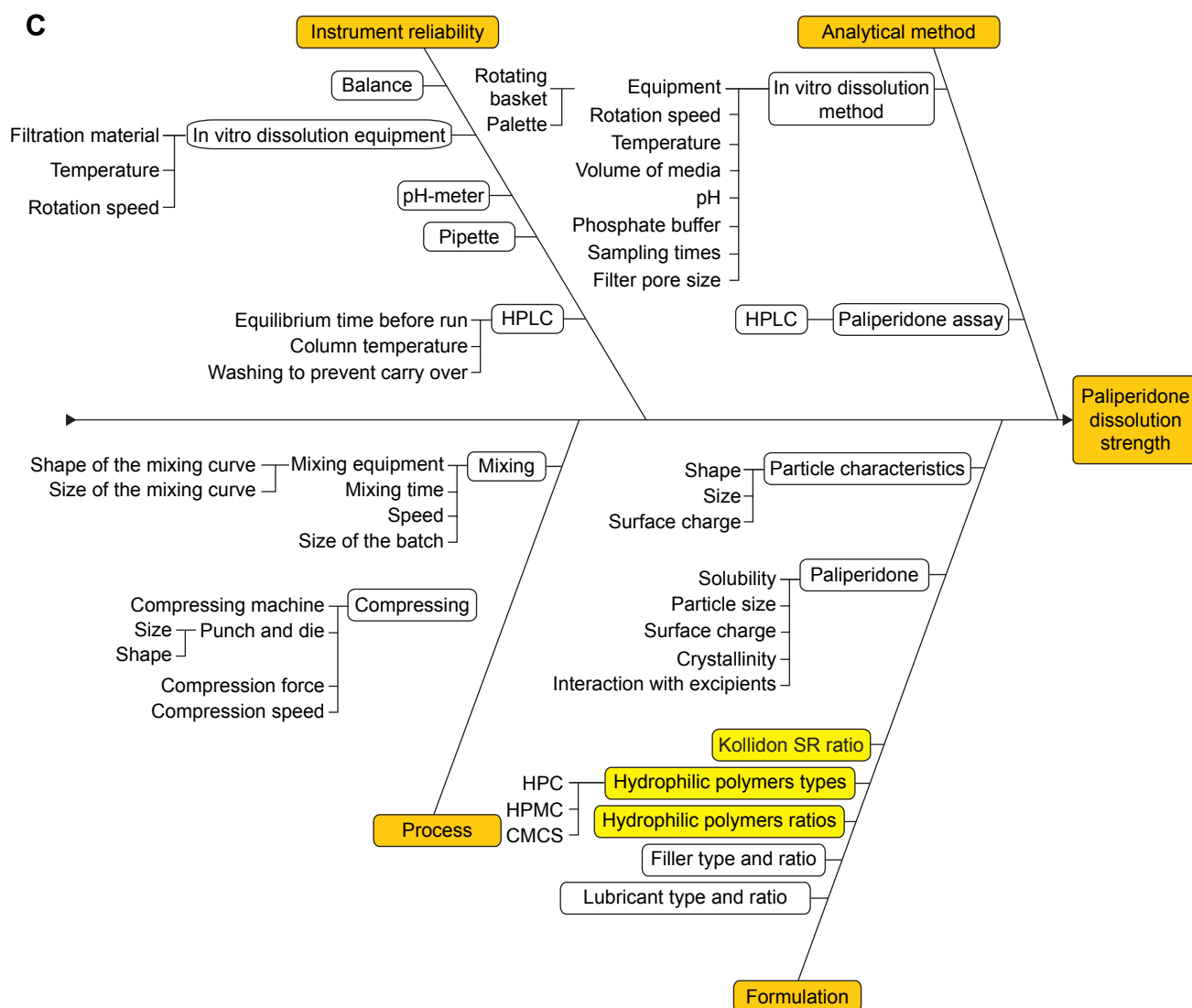


Figure 1 Ishikawa diagrams illustrating factors that may have an impact on weight uniformity (A), crushing strength (B), and the dissolution profile (C).

Abbreviations: CMCS, sodium carboxymethyl cellulose; HPC, hydroxypropyl cellulose; HPLC, high-performance liquid chromatography; HPMC, hydroxypropyl methylcellulose.

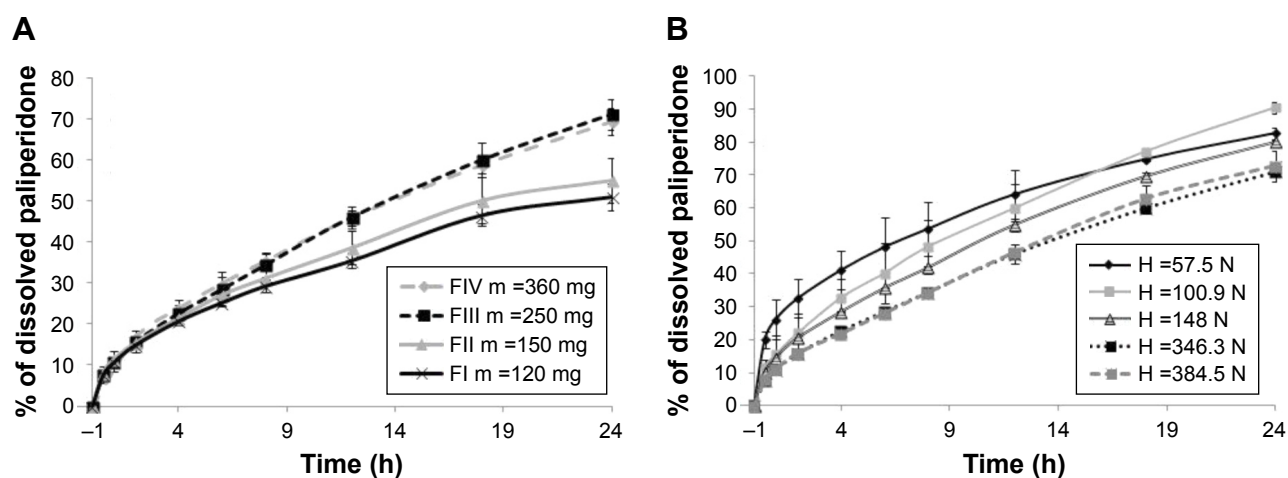


Figure 2 Paliperidone release profiles from the delivery systems illustrating the influence of the tablet weight (A) and the crushing strength (B) on paliperidone dissolution.

Notes: FI, FII, FIII, and FIV are preliminary tablet formulations with compositions described in Table 3. H is crushing strength (N).

DoE

The DoE included the two quantitative formulation parameters whose variations were considered the most hazardous for the quality profile of the final product and were ranked first according to their RPN values: the insoluble polymer, Kollidon SR ratio, and the soluble polymer ratio. Although the type of hydrophilic polymer, once chosen, was not considered a menace to the QTPP of the developed system (RPN=15, meaning low risk), it was included into the experimental design as a qualitative variable, to have a better view on its influence on the release and on its interactions with the insoluble matrix-forming agent.

Apart from the three aforementioned independent variables, the crushing strength was included into the experimental design matrix as a controlled variable, to eliminate/neutralize its influence on the dissolution results.

The results of ANOVA showed whether the variation of the responses was caused by the independent variables or it occurred by chance, at a confidence level of 95%, meaning that a model was considered significant when $P < 0.05$. The statistical analysis (Table 5) revealed highly significant models for all responses, with $P < 0.05$. The regression coefficients were > 0.90 , for most of the responses, which indicates that a high percentage of the response variance was explained by the model. At an R^2 value of 0.90, 90% of the response was explained by the model.²² Adjusted R^2 values were in a reasonable agreement, particularly for the reduced models, signifying good model fit. The Q^2 values > 0.5 and the small differences < 0.2 between R^2 and Q^2 , obtained for ten out of eleven responses, indicate the good predictive power and appropriateness of the developed models.²²

Effects of factors on the Pal dissolution

The results for the measured responses, meaning the percentages of released Pal at different sampling times, were included into the design matrix (Table 4). Table 6 contains the revised regression coefficients for responses Y_1 – Y_9 . The responses, Y_1 – Y_9 , represented the percentage of released Pal at the nine sampling times, from 0.5 to 24 h. The release behavior was primarily influenced by the Kollidon SR ratio, with a negative effect on the dissolution throughout the 24-h test, meaning that the increase in Kollidon SR percentage determined slower Pal dissolution. A denser insoluble matrix with small pores determines low water infiltration and thus slow Pal diffusion into the dissolution media.²³

Figure 3 depicts the influence of quantitative factors for each of the three hydrophilic polymers over time. It was represented in that way, to emphasize the manner the influences

evolve during the dissolution test, for a better understanding of the effects of the variables and their interactions and for a complete image of the factors that control the dissolution mechanism.

During the first hours of the dissolution test, at low Kollidon SR level, HPC percentage increase determined the delay in dissolution, whereas at a high Kollidon SR level, the Pal release was favored by the presence of high ratios of HPC. The same behavior was observed after 4 h, on the whole range of insoluble polymer concentration. In addition, in the first 6 h, at a high HPC content, an inflection point in the Kollidon SR concentration was found, ~32%, up to which the Pal release diminished, but when it was surpassed, the Pal release increased again. Thus, in the first interval of the dissolution test, Kollidon SR influence was the most significant, and higher concentrations led to more compact matrices and low contact surface between Pal and media, which resulted in slow dissolution, but after 6 h, Kollidon SR influence decreased and HPC influence became more significant, accelerating the release by inflating and breakage of the inert matrix.

HPMC influence is important in the first 6 h of the dissolution test and at low Kollidon SR ratios. A 10% increase in HPMC concentration produced a decrease of 30% in Pal dissolution after 30 min. Over the 24 h, the HPMC effect gradually decreased, whereas the Kollidon SR influence became linear. Unlike HPC, HPMC produced a more abrupt delay due to faster hydration that yielded a thick gel, which constituted a barrier for the active principle diffusion. The further gel structure erosion and polymer dissolution that occurred after ~6 h led to the loss of effect on the entire Kollidon SR concentration range.²⁴

CMCS exhibited low effect on dissolution at high levels of Kollidon SR and significantly prolonged Pal release at low ratios of insoluble polymer, with a more significant effect at the beginning of the test. Due to its higher solubility, gel erosion occurred faster, and the dissolution lag was less important compared to the HPMC formulations.²⁵

Effects of factors on the release kinetics

Several kinetic equations including Baker and Lonsdale, Peppas and Korsmeyer, Hixon and Crowell, Higuchi, first order, and zero order were tested in order to assess the Pal release behavior. Table 7 lists kinetics coefficient, Akaike constant, and correlation values. The equation that best fitted the data was Peppas–Korsmeyer ($R^2 > 0.99$), although the Higuchi model also showed good results. Therefore, both mechanisms of erosion and diffusion participated to the Pal release, erosion, and diffusion.

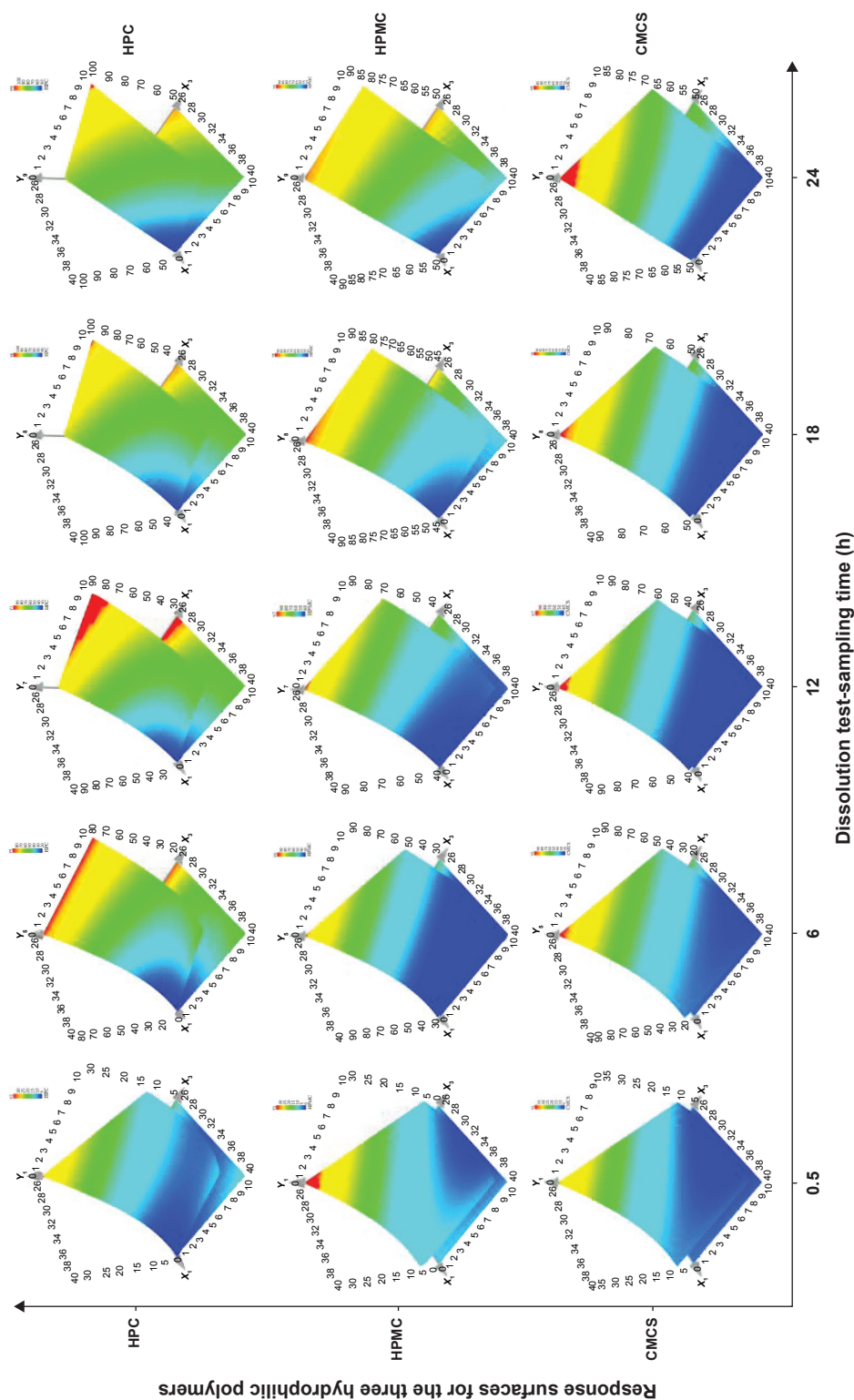


Figure 3 Response surfaces showing the influences of Kollidon® SR ratio (X_1) and hydrophilic polymer ratio (HPC, HPMC, and CMCS; X_2) on paliperidone release after 0.5 (Y_1), 6 (Y_2), 12 (Y_3), 18 (Y_4), and 24 h (Y_5).
Abbreviations: CMCS, sodium carboxymethyl cellulose; HPC, hydroxypropyl cellulose; HPMC, hydroxypropyl methylcellulose.

As R^2 values were high enough to evaluate the dissolution behavior, the diffusional exponents were analyzed to characterize the type of diffusion. Most of the formulations released the active principle by non-Fickian transport (anomalous), with $0.45 < n < 0.89$, especially at high Kollidon SR ratios.^{26,27} The release was done after Fickian transport when small amounts of Kollidon SR were used ($n < 0.45$). The diffusion constant k is a measure of the release rate, and with the diffusion exponent n , it was analyzed as a response in the DoE (Y_{10} and Y_{11} , Table 7).²⁸ The generated response surfaces (Figure 4) showed that the release rate decreased when increasing the ratios of both insoluble and soluble polymers. The diffusion mechanism changed from Fickian to anomalous when Kollidon SR ratios increased. At a maximum Kollidon SR content, adding a hydrophilic polymer (HPMC; Figure 4) produced no effect on the active principle transport mechanism, probably because the rigid porous structure formed by the insoluble polymer did not allow polymer swelling and drug diffusion.^{29,30}

Design space and optimization

Among the different approaches used to establish the design space, this work used response surface methodology with optimization to generate a domain of input variables that lead to a product with the desired CQAs. The statistical effect analysis verified whether the selected formulation

variables and their interactions had a significant effect on Pal release from the delivery systems. The relationships between the CPPs and the CQAs were established by response surface modeling, which allowed the thorough understanding of their interconnections present in the experimental domain. From the initial experimental area, a design space was isolated (Figure 5) where all the specifications stated in the QTPP were met at a certain risk level. In order to generate it, a series of limitations and target values on the responses were applied, as indicated in Table 4. The target values for dissolution profile were selected so as to assure the Pal release according to the identified release mechanism of active ingredient from prepared matrix tablets (erosion and diffusion) for a period of 24 h. The CQAs indicated that the Pal release was constrained to low values at the beginning of the dissolution test and maximized after 24 h. As one of the independent variables was qualitative (the type of hydrophilic polymer), the conditions to obtain the Pal delivery system with the desired release by using HPMC as a hydrophilic matrix agent were generated.

Each point from the design space surface represents a possible different formulation, having the Pal release specified in the QTPP, with a certain risk level. The risk of getting predictions outside the specifications, expressed as defect per million opportunities (DPMOs), was estimated by using Monte Carlo simulations (Figure 5). In order to prove that

Table 7 Release kinetics characteristics of the prepared formulations

Exp	Baker and Lonsdale			Peppas and Korsmeyer				Hixon and Crowell			Higuchi			First order			Zero order		
	R^2	AIC	k	R^2	AIC	$k (Y_{10})$	$n (Y_{11})$	R^2	AIC	k	R^2	AIC	k	R^2	AIC	k	R^2	AIC	k
N1	1.000	10.33	0.054	0.999	17.95	49.62	0.3626	0.956	33.01	0.170	0.979	27.47	41.771	0.980	29.25	0.610	0.702	41.92	19.091
N2	0.996	21.50	0.062	0.991	27.84	52.32	0.3480	0.975	30.58	0.196	0.965	30.34	43.248	0.991	25.64	0.703	0.652	42.93	19.643
N3	0.994	33.29	0.024	0.991	37.89	32.70	0.4327	0.967	45.24	0.071	0.987	36.90	28.796	0.987	38.80	0.261	0.778	57.88	9.717
N4	0.997	30.02	0.004	1.000	17.53	13.89	0.4923	0.930	58.96	0.016	0.999	14.40	13.619	0.954	55.36	0.056	0.852	65.38	3.323
N5	0.987	54.10	0.013	0.995	39.56	22.41	0.5056	0.985	46.22	0.042	0.995	35.60	22.696	0.995	37.70	0.151	0.854	63.64	6.434
N6	0.996	29.05	0.002	0.999	15.02	9.96	0.5177	0.927	54.79	0.011	0.999	14.02	10.418	0.944	52.44	0.036	0.879	59.13	2.558
N7	0.999	26.76	0.006	0.997	35.06	20.34	0.4115	0.886	65.23	0.022	0.987	43.91	16.273	0.927	61.37	0.079	0.724	72.36	3.891
N8	1.000	9.06	0.002	1.000	3.02	11.47	0.4750	0.897	57.78	0.011	0.999	12.43	10.763	0.920	55.59	0.038	0.834	61.76	2.618
N9	1.000	10.33	0.054	0.999	17.95	49.62	0.3626	0.956	33.01	0.170	0.979	27.47	41.771	0.980	29.25	0.610	0.702	41.92	19.091
N10	0.974	50.17	0.011	0.994	40.54	18.00	0.5739	0.993	39.48	0.036	0.990	40.77	21.288	0.999	24.60	0.129	0.907	60.16	6.119
N11	0.994	38.11	0.005	0.995	38.56	14.82	0.4911	0.934	59.95	0.018	0.995	34.71	14.484	0.960	55.53	0.063	0.842	67.35	3.523
N12	0.996	29.05	0.002	0.999	15.02	9.96	0.5177	0.927	54.79	0.011	0.999	14.02	10.418	0.944	52.44	0.036	0.879	59.13	2.558
N13	0.991	40.08	0.003	0.997	33.51	11.64	0.5336	0.947	56.16	0.014	0.996	31.79	12.680	0.967	52.08	0.050	0.885	62.92	3.115
N14	1.000	10.33	0.054	0.999	17.95	49.62	0.3626	0.956	33.01	0.170	0.979	27.47	41.771	0.980	29.25	0.610	0.702	41.92	19.091
N15	0.995	37.31	0.005	0.992	43.46	17.84	0.4367	0.894	64.08	0.019	0.987	43.46	15.204	0.933	60.23	0.069	0.763	70.73	3.648
N16	0.998	24.44	0.003	0.998	25.46	11.44	0.4879	0.908	57.72	0.012	0.998	22.08	11.099	0.932	55.17	0.040	0.844	62.22	2.702
N17	0.996	29.05	0.002	0.999	15.02	9.96	0.5177	0.927	54.79	0.011	0.999	14.02	10.418	0.944	52.44	0.036	0.879	59.13	2.558
N18	0.997	27.43	0.003	0.999	17.69	10.92	0.5079	0.925	56.34	0.012	0.999	14.31	11.146	0.945	53.62	0.040	0.867	61.18	2.727
N19	1.000	13.31	0.004	1.000	7.83	15.11	0.4311	0.868	62.11	0.014	0.994	32.24	12.694	0.901	59.67	0.049	0.771	66.59	3.057
N20	0.999	17.75	0.003	0.999	21.69	11.64	0.4770	0.898	58.21	0.012	0.998	20.67	10.980	0.923	55.86	0.039	0.832	62.40	2.667
N21	0.997	26.42	0.003	0.999	21.49	11.09	0.5021	0.920	56.84	0.012	0.999	17.51	11.144	0.941	54.16	0.040	0.860	61.57	2.722

Notes: Y_{10} , k -Peppas; Y_{11} , n -Peppas.

Abbreviations: AIC, Akaike information criterion; Exp, experiment.

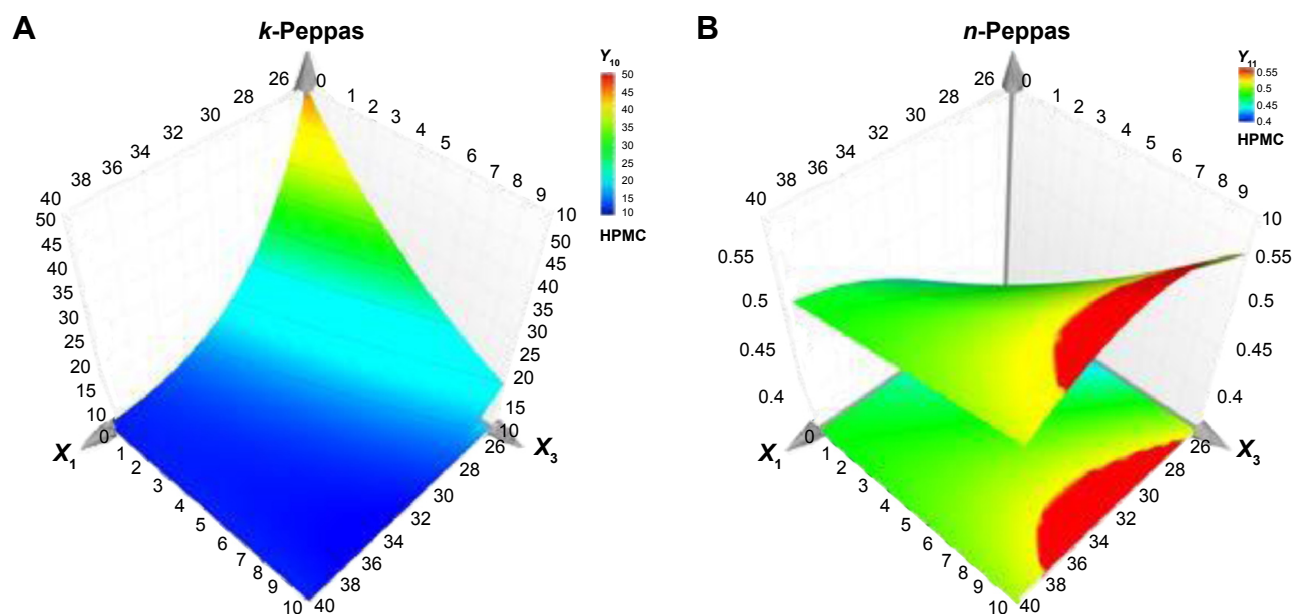


Figure 4 Response surfaces showing the influences of Kollidon® SR ratio (X_1) and hydrophilic polymer ratio (HPMC) (X_3) on paliperidone release kinetics expressed as (A) *k*-Peppas (Y_{10}) and (B) *n*-Peppas (Y_{11}).

Abbreviation: HPMC, hydroxypropyl methylcellulose.

the model fits the data satisfactorily for predicting the drug release, the optimizer option of the Modde software was used to select an optimal formulation from the design space that contained $X_1=27.62\%$ Kollidon SR, $X_2=$ HPMC, and $X_3=8.73\%$ HPMC. The optimal formulation was prepared and tested under the same conditions as the former experimental runs. The small differences between the experimental results and the predicted ones, calculated as residuals (Table 4) and a *P*-value of 0.824, prove the validation of revised models, meaning that the process produces the desired CQAs if operated within the design space.

Risk mitigation and control strategy

Ishikawa diagrams and FMEA were used to establish a hierarchy of the input variables with the highest risks on Pal release. The factors with the highest impact were studied by using DoE, which resulted in the development of a design space, as an acceptable region within which the quality of the product can be assured, as stated in the QTPP. The risk mitigation and control strategy consists in a series of measures of quality assertion based on product and process knowledge.²¹

The variable X_1 had an important impact on Pal release from the delivery system, as shown in regression equation

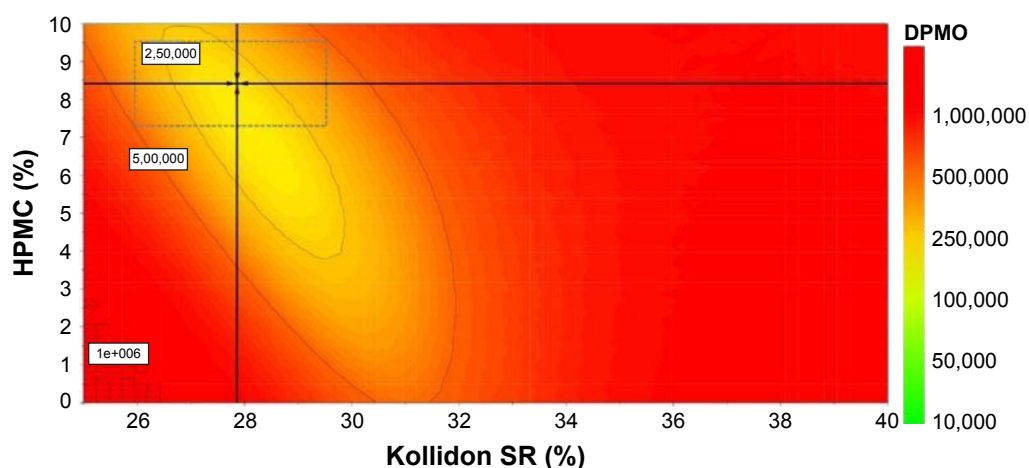


Figure 5 The design space for the paliperidone prolonged release systems that meet the specifications in the QTPP, expressed as DPMOs as a function of X_1 (Kollidon SR ratio) and X_3 (hydrophilic polymer ratio, HPMC) quantitative variables.

Abbreviations: DPMOs, defect per one million opportunities; HPMC, hydroxypropyl methylcellulose; QTPP, quality target product profile.

coefficients (Table 6), response surfaces (Figure 3), and the *P*-value from ANOVA (Table 5). As discussed earlier, there is an optimum ratio of Kollidon SR, but also a wider range around the value of 27.62% where the desired release can be achieved. Keeping the variable X_1 in this range assures Pal dissolution in the constraints range with a low error risk.

The type of hydrophilic polymer and especially the hydrophilic polymer ratio (X_2 and X_3) were ranked as highly important failure modes by the FMEA. The DoE results confirmed their impact (Table 6; Figure 3). Of the three evaluated polymers, HPMC was efficient in counteracting the burst release of Pal. Moreover, HPMC percentage variation produced the lowest effect on Pal release; therefore, it was selected as a hydrophilic matrix agent in the optimal formulation. The optimal formulation contained 8.73% HPMC, and moderate variations from this value were not expected to produce any significant effect on active ingredient dissolution.

The other two failure modes, punch and die size and compression force, were optimized in the preliminary part of the study, and in a validated production process, variation in these modes was most unlikely to occur.

Working within the established range of the process and formulation parameters leads to low failure-mode risks. However, the risk mitigation strategy involves monitoring the Pal release and maintaining the Pal dissolution parameters within the constraint range.

Conclusion

The current study demonstrated the relevance of the application of quality by design concept in the development of a new pharmaceutical product. An inert matrix based on Kollidon SR was developed, having HPMC as a hydrophilic polymer to modulate Pal release, through a highly predictive model with a small number of experiments. A formulation containing 27.62% Kollidon SR and 8.73% HPMC was found as the most promising with respect to both drug release and potential risks regarding quality assurance.

The risk analysis of failure modes coupled with experimental design proved their utility by outlining the parameters that have a high impact on product quality and establishing safe ranges for their variation. Such an approach can be of high importance when fast development of a product is requested, for expensive processes or simply to avoid getting products outside the specifications.

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Disclosure

The authors report no conflicts of interest in this work.

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