Effect of ultrafine poly(ε-caprolactone) fibers on calcium phosphate cement: in vitro degradation and in vivo regeneration

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Abstract: We incorporated ultrafine polymer fibers into calcium phosphate cement (CPC) to improve the resorption rate of CPC with fiber degradation. Different weight percentages of electrospun poly(ε-caprolactone) fibers (0%, 3%, and 7%, named as ultrafine fiber-incorporated CPC0 [UFICPC0], UFICPC3, and UFICPC7) were included into preset CPC specimens for in vitro immersion in lipase phosphate-buffered solution and long-term in vivo implantation in the femoral condyle of rabbits. The effect of the ultrafine poly(ε-caprolactone) fibers with a diameter ranging from nanometer to micrometer on CPC degradation was evaluated by measuring the pH of the medium, mass loss, porosity, and physiochemical properties. For the in vitro evaluation, histomorphometrical analysis as well as three-dimensional (3D) reconstruction was applied to assess the osteo- genic properties of the CPC composite. After in vitro immersion and in vivo implantation, the total porosity and macroporosity as well as the bone formation and ingrowth increased significantly during time in the fiber-incorporated CPC specimens. After 24 weeks of implantation, the degraded space was occupied by newly formed bone, and the UFICPC3 and UFICPC7 composites showed a ~3.5 times higher fraction of bone volume than that of the pristine CPC (UFICPC0). In vitro and in vivo results proved that the introduction of ultrafine degradable fibers within a CPC matrix can be used to improve macroporosity efficiently and enhance CPC degradation and bone ingrowth largely.

Keywords: ultrafine fibers, calcium phosphate cement, macroporosity, degraded space, bone ingrowth

Introduction

Calcium phosphate cements (CPCs) have gained clinical acceptance to repair a bone defect due to their recognized bioactivity and moldability.1 Typical applications are the treatment of maxillofacial defects or deformities and augmentation of spine.2 The material can even be applied by using minimally invasive surgery and for the filling of complex-shaped defects.3 However, two major drawbacks limit their clinical use. One is the inherent brittleness derived from the composition and microstructure.4 The other is the slow resorption rate.5,6

The incorporation of bioresorbable or biodegradable materials into the CPC matrix can circumvent these two drawbacks. Fiber reinforcement of CPC is the most successful approach to toughen this brittle material.1 Various fibers have already been used for such a purpose, such as ceramic fibers (eg, carbon or glass fibers), nonresorbable polymer fibers, and resorbable polymer fibers (eg, polylactide, polyglycolide/polylactide copolymers, poly-ε-caprolactone [PCL], etc).7 When bioresorbable or biodegradable fibers are used, this will not only contribute to the initial mechanical strength, but also
porosity will be created after fiber degradation. The porosity will increase the surface area of CPC matrix, resulting in increased resorption of the cement and facilitation of bone ingrowth.

Most of the articles dealing with degradable fiber-reinforced CPC focus on the mechanical properties and cell response. Only a few report about the long-term in vivo behavior.\(^8\)\(^-\)\(^10\) The results of these studies are contradictory on the efficient of degradable fibers addition. For example, in a 52-week study dealing with poly(lactic-co-glycolic acid) (PLGA) fiber-reinforced CPC, fiber degradation could not be associated with a promising bone regeneration.\(^9\) In another in vivo study, a porous material transferred from the CPC/PLGA composite exhibits a perfect osteoconduction accompanied with osteoblast-like cells and Haversian canals after 24-week implantation.\(^10\) Therefore, further in vivo studies should be carried out to obtain more data on degradation and bone regeneration of fiber-reinforced CPC.

Besides commercial fibers in the range of 10–120 µm, ultrafine electrospun fibers (0.5–2 µm) have been used to build scaffolds for bone tissue engineering to mimic the nanofibrous collagen network of the bone matrix.\(^11\) Such ultrafine fibers have several attractive characteristics, as higher specific surface area and superior mechanical performance, compared with any other regularly formed material.\(^12\)

However, a scaffold prepared from such fibers is not rigid enough to withstand the mechanical stresses during bone tissue neogenesis. Therefore, in a previous study, we prepared and evaluated a series of CPC composites reinforced with electrospun biodegradable fibers on mechanical properties, porosity, and morphological structure.\(^13\) The results indicated that the incorporation of ultrafine fibers enhanced the fracture resistance and porosity of CPC. In particular, the work of fracture of CPC composites with 7 wt% PCL fibers increased dramatically, which is approximately 30 times higher than that of pristine CPC.

In this study, we aim to further investigate the effects of ultrafine PCL fibers on their biodegradation and osteogenetic properties by both in vitro and in vivo evaluation. For the in vitro degradation assay, enzyme containing medium was used to partly mimic the physiological environment. The effect of the PCL fibers with a diameter ranging from the nanometer to micrometer scale on CPC degradation was evaluated by measuring the pH of the medium, mass loss, porosity, and physiochemical properties. For the in vivo evaluation, histomorphometrical analysis as well as three-dimensional (3D) reconstruction were applied to assess the bioresorption and the bone regeneration of the composite materials.

### Materials and methods

#### Materials

The CPC powder (Calcibon\(^\text{®}\)), consisting of 61% α-tricalcium phosphate (TCP), 26% CaHPO\(_4\), 10% CaCO\(_3\), and 3% precipitated hydroxyapatite (HA), was provided by Biomet Merck (Berlin, Germany). The cement liquid applied was a 1% aqueous solution of Na\(_2\)HPO\(_4\). PCL with an average molecular weight of 80,000 was purchased from Sigma-Aldrich (St Louis, MO, USA). Lipoprotein lipase (Lipase PS Amano SD, Lot TLK0015, Wako Pure Chemical Industries, Ltd, Osaka, Japan) was dissolved in phosphate buffer solution (PBS) (pH = 7.4) to enzymatically degrade PCL fibers and CPC composites.

#### Preparation of PCL fiber bundles

Ultrafine PCL fibers were fabricated by electrospinning using a special water pool technique as previously described.\(^13\) Briefly, PCL granules were dissolved in tetrafluoroethylene to obtain 12% (w/v) polymer solution under gentle stirring for 12 hours. A commercially available electrospinning apparatus (Advanced Surface Technology, Bleiswijk, the Netherlands) was used for the fiber bundles fabrication. Upon applying a high voltage of 18.15 kV, PCL solution was ejected from a needle (inner diameter of 0.8 mm) by feeding from a glass syringe at a rate of 1.5 mL/h. The polymer jet was directed to a grounded water pool positioned under the needle at a distance of 28 cm, and the charged polymer fibers were deposited on the surface of water. Then, the random fibers were drawn to a rotating mandrel (diameter of 4.5 mm) at a speed of 12 rpm to form an oriented fiber bundle (diameter of single fibers were ranging from 400 to 1,100 nm). The collected fiber bundles (Φ0.2 mm) were freeze-dried for 24 hours, then cut into pieces of 3 mm in length, and stored at −20°C.

#### Preparation of cement/fiber composites

CPC powder and 1% (w/v) Na\(_2\)HPO\(_4\) solution were mixed inside a 2 mL plastic syringe and subjected to a vigorous shaking for 15 seconds (YDM mixing apparatus, Hangzhou Xinya Co. Ltd, Hangzhou, People’s Republic of China). A liquid/powder (L/P) ratio of 0.33 was applied. After shaking, the mixture in a paste form was immediately injected into a container and blended manually by a spatula with the cut electrospun fiber bundles. The weight fractions of the fibers were 0%, 3%, and 7%, respectively. Then, the fiber–paste mixture was filled into a Teflon mold of 5×5 mm\(^2\) and gently pressed with a spatula. The composite mixture in the mold was covered with a glass slide and stored at 37°C.
in a humidor for 24 hours. Then the hardened composite specimens were taken out from the mold and vacuum dried for testing.

For convenience, the ultrafine fiber-incorporated CPC (UFICPC) with fiber weight fractions of 0%, 3%, and 7% were named as UFICPC0, UFICPC3, and UFICPC7, respectively. The fiber volume of UFICPC3 and UFICPC7 composites has been calculated by:

$$v \% = \frac{\rho_{HA} \times \text{wt} \%}{\rho_{PCL}},$$  

(1)

where $\rho_{HA}$ = 3.156 g cm$^{-3}$, $\rho_{PCL}$ = 1.145 g cm$^{-3}$, $v$ means fiber volume, wt means fiber weight.

**In vitro degradation**

For the enzymatic degradation studies, three groups of preset UFICPC specimens (UFICPC0, UFICPC3, and UFICPC7) and electrospun PCL fibers (100 mg each) were immersed in a vial filled with a lipase solution consisting 5 mL PBS (pH = 7.4) with 200 unit/mL lipoprotein lipase (Lipase PS, Wako Pure Chemical Industries, Ltd) for up to 7 days. The vials were placed in water bath thermostated at 37°C for up to 7 days. The vials were removed from the immersion medium, and vacuum dried over 1 week at 37°C. The pH value of residual solution in each vial was collected and measured by pH meter (n = 3) at each timepoint, referring to the earlier study for degradation of PCL, to observe whether the acidic compounds degraded from PCL would cause the condition change of CPC hydrolysis and degradation.

**pH measurement**

The pH value of residual solution in each vial was collected and measured by pH meter (n = 3) at each timepoint, referring to the earlier study for degradation of PCL, to observe whether the acidic compounds degraded from PCL would cause the condition change of CPC hydrolysis and degradation.

**Morphology observation**

Before degradation, porous structure and fiber distribution of specimens were visualized by microcomputerized tomography (micro-CT) (uCT100, SCANCO Medical AG, Brütisellen, Switzerland) at a resolution of 2.4 µm per pixel. Acquisition parameters for the scanning were 70 kV and 85 µA. The region of interest (ROI) in which the porosity was measured and defined as a cylindrical area covering preset specimen of a $5 \times 5 \text{mm}^2$. The morphology of blade-cut cross-section of specimens before mixed (scanning electron microscope [SEM], Jeol 6310, JEOL Ltd, Tokyo, Japan) and after composite degradation for 1, 3, and 7 days was observed using a SEM (JSM-6500LV, JEOL Ltd). Samples were sputter-coated with gold prior to observation.

**Mass loss test**

In order to characterize the degradability, the composite weight was measured after removal from the immersion medium, and vacuum dried over 1 week at 37°C. Mass loss was determined using Equation 2:

$$R_L = \frac{m_n - m_0}{m_0} \times 100\%,$$  

(2)

where $R_L$ is the mass loss of the sample (%) on $t = n$, $m_0$ is the mass of the sample (g) on $t = 0$, $m_n$ is the mass of the sample (g) when $t = n$.

**Porosity determination**

The porosity of preset CPC specimens containing PCL fibers was determined according to the method described previously. In brief, the UFICPC composites were weighed before and after burning out PCL fibers at 400°C for 2 hours. Equations 3 and 4 were used for the calculation of the total porosity and the macroporosity:

$$\varepsilon_{\text{tot},n} = \frac{1 - \frac{m_{\text{burnt},n}}{V \times \rho_{HA}}}{100\%}$$  

$$\varepsilon_{\text{macro},n} = \frac{1 - \frac{m_{\text{burnt},n}}{m_{\text{micro},n}}}{100\%},$$  

(3)

where $\varepsilon_{\text{tot},n}$ is total porosity (%) when $t = n$, $\varepsilon_{\text{macro},n}$ is macroporosity (%) when $t = n$, $m_{\text{burnt},n}$ is the mass (g) of UFICPC composite after burning when $t = n$, $V$ is the volume of the sample (cm$^3$), $\rho_{HA}$ is the density of HA (3.156 g/cm$^3$), $m_{\text{micro},n}$ the average mass (g) of the pristine CPC sample after burning when $t = n$. Tests were performed triplicate.

**Phase composition analysis**

Three groups of UFICPC samples before degradation as well as after degradation for 1 and 7 days were ground for testing. The structure of the CPC composites was studied by X-ray diffraction (XRD, DX2500, Dandong Fangyuan Instrument LLC, Dandong, People’s Republic of China) to determine the phase composition, relative intensity of crystalline PCL in composites, and the phase conversion of CPC. The X-ray generator was operated at a voltage of 40 kV with a tube current of 25 mA. The diffraction pattern was recovered by a proportional counter in the angular range from $2\theta = 10^\circ$ to $70^\circ$.
using a step width of \( \Delta(2\theta) = 1^\circ \). The same ground samples were also used for Fourier transform infrared spectroscopy (FTIR, Nicolet 6700, Thermo Fisher Scientific, Waltham, MA, USA). The typical PCL absorption band and calcium phosphate band of the UFICPC composite were measured over a wavenumber range of 400–4,000 cm\(^{-1}\) with a KBr sample weight ratio of 100/1.

**In vivo experiment and evaluation**

The animal experiment was approved by the Animal Ethical Committee of Sichuan University and performed as per the China national guidelines for the care and use of laboratory animals. Thirty-six healthy adult New Zealand White rabbits (18 males and 18 females), weighing 2.2–3.0 kg, were divided randomly into three experimental groups. Anesthesia was induced by ear vein injection of 3% sodium pentobarbital at a dose of 1 mL/kg. The hind limbs of rabbits were shaved, washed, and disinfected with povidone-iodine. A cylindrical bone defect (diameter 5.5 mm, depth 5 mm) was drilled on the left side after exposure of the distal femoral condyle.

Specimens of UFICPC0, UFICPC3, and UFICPC7 were implanted into the created condylar defects of three experimental groups, respectively. Postoperative animals were allowed freedom of movement, and daily intramuscular injection of penicillin and gentamicin was given for 3 days to prevent infection. The implantation periods were set for 4, 8, 12, and 24 weeks. At each time point, three rabbits were in each group. At each timepoint of implantation, rabbits were sacrificed with an overdose of anesthesia and samples of 4, 8, and 12 weeks were harvested for histological evaluation. Only the harvested samples of 24 weeks were evaluated by micro-CT analysis.

**Microcomputed tomography analysis**

Three-dimensional analysis was conducted on the 24 samples using a vivaCT40 micro-CT imaging system (SCANCO Medical AG). In brief, each sample was placed with its long axis in the vertical position, and immobilized with a foam pad in a cylindrical sample holder for scanning. The femoral condyles of each sample were scanned. A ROI of 5 mm in diameter was defined to cover the created defect. The same ROI was used in all the samples. The scanning system was set at 70 kV, 114 \( \mu \)A, and 8 W; a total of 300 microtomographic slices with a slice increment of 20 \( \mu \)m were taken for each sample. 3D Gaussian filter was constrained at \( \sigma = 1.2 \) and support \( = 2 \) for partial suppression of the noise in the volumes. A threshold equal to or above 401 represented the CPC component; a threshold below 401 and equal to or above 270 signified the bone tissue; a threshold below 270 represented the marrow and soft tissue. \(^{16,17}\) The 3D reconstructed images were acquired from a series of 130 serial 2,048×2,048 bitmap images. In addition to the visual assessment of structural images of bone and cement, morphometric parameters were determined from the microtomographic datasets using direct 3D morphometry, including the fraction of bone volume/tissue volume (BV/TV), material volume (MV)/TV, and trabecular number (Tb. N).

**Histological examination**

During the study, the tissue-covered specimens were retrieved and fixed in 10% formalin. Preliminarily, one series of specimens at different interval times were decalcified in buffered formic acid for 7 days at room temperature and embedded in paraffin. After the paraffin-embedded specimens were cut into slices and stained with hematoxylin/eosin, the decalcified sections were observed under optical microscope. Due to the fact that the major components of testing materials were inorganic CPC, the implant sections were fragmented and could not provide enough information of the study. Hence, only two serial specimens were dealing with embedding undecalcified bone method for further histological investigation. In this regard, the statistical analysis of animal testing could not be practiced without enough samples in this paper.

Therefore, the harvested samples of 4, 8, and 12 weeks were fixed in 4% formaldehyde for 1–2 weeks, then dehydrated in graded ethanol solution, and embedded in methylmethacrylate. Nondecalcified cross-sections of the embedding specimens were prepared using Leica SP1600 hard tissue slicer. The ultrathin sections (\( \sim 100 \) \( \mu \)m) were stained with methylene blue and basic fuchsin and examined via a light microscope.

**Statistical analysis**

SPSS software was used to establish a database and statistical analysis, the data from in vitro test were expressed as mean ± standard deviation. Statistical significance was determined by the \( P \)-value of Student’s \( t \)-test, \( P<0.05 \) indicates statistically significant. The data for one-way analysis of variance were analyzed via a Tukey multiple comparison test.

**Results**

**Effect of enzymatic degradation on pH value in vitro**

The pH values of the enzymatic media were measured at different immersion times, as shown in Figure 1. The release of
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acidic products from the pure PCL fibers in the medium results in a faster decrease of pH value from 7.4 to 4.8 in 4 days (Figure 1A). Thereafter, the pH value decreased slowly to 4.5 at day 7. The UFICPC composites with or without ultrafine PCL fibers showed a similar trend, but with a relatively slower rate, ie, the pH on day 7 is still above 6.5 (Figure 1B). The pH values of the enzymatic media for the ultrafine fiber-reinforced composites (UFICPC3 and UFICPC7) are lower than the pristine CPC (UFICPC0). At 1, 3, and 5 days of incubation, the pH values of the enzymatic medium for the 3 and 7 wt% fiber fractions differed significantly (P<0.05), but this difference did not exist at day 6 and 7.

Effect of enzymatic degradation on morphology and porosity

Cross-sectional micro-CT images were obtained from all materials (Figure 2B–D). Small air bubbles or small pores were visible as black color in the materials. Density morphology was presented in the UFICPC0 sample (Figure 2B). Ultrafine PCL fibers in the UFICPC3 and UFICPC7 cement could be clearly recognized (dark gray-black elongated structures) and also some irregular-shaped cracks (black color) were observed (Figure 2C and D). Interconnected and tangled fiber-like morphologies dispersed in the compact cement matrix. Table 1 lists fiber volumes and porosities of composites that have been calculated from different theories.

The SEM micrographs in Figure 2A show a fibrous structure with a diameter ranging from nanometer to micrometer, and Figure 3 demonstrates a progressive fiber degradation of the composites in the lipase PBS. The UFICPC0 specimens showed the presence of some surface microporosity. No apparent degradation of the UFICPC0 specimens was observed. On the other hand, it seemed that some additional deposition of material occurred during incubation for the chemical conversion of calcium and phosphate ions (Figure 3A–D). For sample UFICPC3 and UFICPC7 specimens, besides conversion of the CPC matrix, the PCL fibers became thinner from micrometer to nanometer with time and a lot of fibers had completely disappeared on day 7, leaving many fiber traces (grooves) in the CPC matrix (Figure 3, E–H for UFICPC3, I–L for UFICPC7).

The weight change of pure PCL fibers and UFICPC cements in lipase PBS solution is plotted in Figure 4. Pure PCL fibers degraded faster in the enzymatic solution than in pure PBS. The mass loss increased rapidly with time and reached approximately 55% on day 7 (Figure 4A). The UFICPC0 samples (pristine CPC cement) showed a slight weight increase during incubation (Figure 4B, 0 wt% curve), indicating a deposition of some component in enzymatic PBS solution on the CPC matrix. The UFICPC3 and UFICPC7 specimens showed a linear decrease in mass after 1 day of incubation, but mass loss was much lower compared with pure PCL fibers. Compared to UFICPC3, UFICPC7 specimens showed a significantly higher mass loss (P<0.05).

By means of the burning-out method, the total porosity and macroporosity of composite cements at different immersion times are calculated and shown in Figure 5. It can be seen that both the total porosity and macroporosity increase with the immersion time, sample UFICPC7 holds higher porosities than samples UFICPC3 and UFICPC0. Significant difference in microporosity is present between UFICPC7 and UFICPC3, and among UFICPC7, UFICPC3, and UFICPC0 in total porosity. After immersion, the macroporosities of UFICPC3 and UFICPC7 change from starting 10.23% and 19.21% to final...
Table 1 Fiber volumes and porosities of composites by theoretical calculation and micro-CT

<table>
<thead>
<tr>
<th>Specimens</th>
<th>Theoretical calculation</th>
<th>Calculation by Micro-CT</th>
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<tbody>
<tr>
<td></td>
<td>Fiber content (wt%)</td>
<td>Fiber volume (vol%)</td>
</tr>
<tr>
<td>UFIcPc0</td>
<td>0</td>
<td>0</td>
</tr>
<tr>
<td>UFIcPc3</td>
<td>3</td>
<td>8.27</td>
</tr>
<tr>
<td>UFIcPc7</td>
<td>7</td>
<td>12.29</td>
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Note: The calculated data from micro-CT were different with theoretical calculation.

Abbreviations: CPC, calcium phosphate cement; CT, computed tomography; UFICPC, ultrafine fiber-incorporated CPC.

15.0% and 24.5% on day 7, which is almost two times higher than the calculated fiber volume (8.27% and 12.29%).

Effect of enzymatic degradation on phase composition

The XRD patterns in Figure 6B and C show that the monetite and \( \alpha \)-TCP phase composition in UFIcPc3 and UFIcPc7 converts progressively into apatite within 7 days, which is faster than the conversion of pristine CPC (Figure 6Bf and Ci vs Ac). After 7 days, both the monetite and \( \alpha \)-TCP components can still be observed in UFIcPC0 (Figure 6Ac).\(^\text{15,18}\) As the content of ultrafine PCL fibers is very small (3 and 7 wt%), only a weak characteristic peak of PCL component located approximately 22° can be found in samples UFIcPc3 and UFIcPc7. This peak becomes weaker or disappears completely during incubation from day 1 to 7 in lipase PBS.

Figure 2 Morphology observation of ultrafine PCL fibers and UFICPC composites.

Notes: (A) SEM micrographs of electrospun ultrafine fibers, which were prepared from 12% (w/v) PCL solutions and collected by water pool with a nano to micro fibrous structure. Micro-CT cross-sectional images of sample UFIcPc0 (B), UFIcPc3 (C), and UFIcPc7 (D). Black colored area was distinguished as small air bubbles or small pores in the CPC by micro-CT machine. Fiber-like morphologies in the UFIcPc3 and UFIcPc7 cement could be clearly recognized as dark gray–black elongated structures. Irregular-shaped black colored area indicates cracks between fibers and cement.

Abbreviations: CPC, calcium phosphate cement; CT, computed tomography; PCL, poly(\( \varepsilon \)-caprolactone); SEM, scanning electron microscope; UFICPC, ultrafine fiber-incorporated CPC.
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Figure 3 SEM micrographs of UFICPC0 (A–D), UFICPC3 (E–H), and UFICPC7 (I–L) before and after immersion in lipase PBS: before immersion (A, E, I), after immersion for 1 day (B, F, J), 3 days (C, G, K), and 7 days (D, H, L).

Notes: No apparent degradation was observed from the UFICPC0 specimens besides surface microporosity (A–D). The PCL fibers became thinner with time and a lot of fibers had completely disappeared on day 7, leaving many fiber traces (grooves) in the CPC matrix (E–L). Bar: 10 µm.

Abbreviations: CPC, calcium phosphate cement; PBS, phosphate buffer solution; PCL, poly(ε-caprolactone); SEM, scanning electron microscope; UFICPC, ultrafine fiber-incorporated CPC.
Figure 7 shows the infrared spectra of three UFICPC composites before and after immersion in enzymatic PBS. The chemical groups of pristine CPC cement (UFICPC0) do not show an obvious change after immersion for 1 and 7 days (Figure 7A). For UFICPC3 and UFICPC7 composites (Figure 7B and C), the peak at 1,729 cm\(^{-1}\) represents the amorphous phase of PCL, and the peaks at 1,298, 1,192, and 735 cm\(^{-1}\) represent the crystalline phase of PCL. The peak at 1,729 cm\(^{-1}\) corresponds also to the C=O stretch of PCL and decreases significantly in intensity during incubation time, which indicates a preferred enzymatic degradation of the amorphous PCL segments. All other peaks are similar to pristine CPC cement and correspond with the phosphate, hydroxyl and carbonate groups. The set CPC matrix contains a carbonated HA structure.

**Histological analysis**

Representative histological images are shown in Figure 8. Bone apposition on the pristine CPC cement (UFICPC0, Figure 8A) surface without any fibrous encapsulation was shown in three periods. Fibrous encapsulation occurred for all ultrafine fiber-incorporated samples (UFICPC3 and UFICPC7, Figure 8B and C). Moreover, the peripheral area of UFICPC7 showed an apparent fracture, as characterized by an irregular surface contour of the composite material. Compare to pristine UFICPC0, plenty of inflammatory cells have been found at the interface of tissue and composite (UFICPC3 and UFICPC7) in Figure 8B and C.

At 4 weeks after implantation, pristine CPC samples (UFICPC0, Figure 8Aa) revealed a more dense structure than
Figure 6 XRD patterns of UFICPC composites before (a, d, g) and after immersion in enzymatic PBS for 1 day (b, e, h) and 7 days (c, f, i): (a–c) for UFICPC0 (A), (d–f) for UFICPC3 (B), and (g–i) for UFICPC7 (C).

Notes: The monetite and α-TCP phase composition of fiber-incorporated composites (B and C) disappeared and converted to apatite phase faster than pristine CPC cement (A). A: apatite, *: monetite, α: α-TCP, arrow: PCL.

Abbreviations: CPC, calcium phosphate cement; PBS, phosphate buffer solution; PCL, poly(ε-caprolactone); TCP, tricalcium phosphate; UFICPC, ultrafine fiber-incorporated CPC; XRD, X-ray diffraction.
other two composites (UFICPC3 and UFICPC7, Figure 8Bb and Cc). At 8 weeks, the sample diameter of pristine CPC cement (Figure 8Ad) has no remarkable change in comparison with the shrinking area of UFICPC3 and UFICPC7 (Figure 8Be and Cf). With increasing time, thicker fibrous capsule has been observed, as shown in Figure 8B and C (UFICPC3 and UFICPC7) with more composites degraded. More broken pieces were separated from composite bulk by fibrous tissue (FT) and bone-like tissue ingrowth. At 12 weeks, the size of the all three samples becomes smaller, but the degradation happened inside of samples UFICPC3 (Figure 8Bh and Ci, vs Ag) and UFICPC7 in contrast to the peripheral areas of UFICPC0. Notably, fibrous capsule occupied the channel-like area and more new bone (NB) invaded into the cement gaps. For samples UFICPC3 and UFICPC7 (Figure 8Bh and Ci), some divided fragments disappeared when bone-like tissue weaved in the degraded area. The observation and definition of bone-like tissue were referenced from similar histological phenomena in previous studies.19,20

The histological results indicate that fiber-incorporated CPC composites have faster degradation properties and more bone-like tissue fabrication interior compared to the pristine CPC cement. FT and NB incised and encompassed the cement remnants, which have been presented in Figure 9, at 12 weeks. Composite (C) was surrounded by a lot of macrophages (M, yellow arrows). As expected, multinucleated giant cells (yellow dash arrow) appeared at the surface of the composite, meaning a phagocytic process happened.

**Micro-CT reconstruction and quantification**

Micro-CT images were utilized for reconstruction and quantification of material degradation. The reversed 3D porous structure reconstructed by the shadow (holes and fiber bundles) of each sample is shown in Figure 10A–C.
Figure 8 Representative histological section of three UFICPC composites, (A) UFICPC0, (B) UFICPC3 and (C) UFICPC7, after implantation for 4 (a–c), 8 (d–f) and 12 weeks (g–i).

Note: Dotted circle covers original area of samples (Φ5 mm), arrow (→) indicates the fibrous capsule wall, and *shows the ultrafine PCL fibers.

Abbreviations: C, composite; CPC, calcium phosphate cement; FT, fibrous tissue; NB, new bone; PCL, poly(ε-caprolactone); UFICPC, ultrafine fiber-incorporated CPC; wk, weeks.

Figure 9 Representative histological section of the fiber-reinforced composites after 12 weeks on implantation.

Notes: (A) Ingrowth of NB into degraded composite was visible. Composite surrounded by macrophages (yellow arrows). (B) A multinucleated giant cell (yellow dashed arrow) appears at the surface of the composite which also has been visualized in (A). Yellow arrows indicate macrophages; Yellow dashed arrow indicates a multinucleated giant cell.

Abbreviations: C, composite; FT, fibrous tissue; M, macrophage; MNGC, multinucleated giant cell; NB, new bone.
Compared to sample UFICPC0 (Figure 10A) with many small pores (black dots) inside and some larger pores (green, yellow, and red area) on the surface, samples UFICPC3 (Figure 10B) and UFICPC7 (Figure 10C) exhibit more and larger pore volume and interconnected channel-like pores throughout the shell and core due to the incorporated ultrafine PCL fibers or fiber bundles.

After 24 weeks of implantation, only the surface of pristine CPC cement is surrounded by bone tissue (blue color), the CPC degradation is slow and limited to the peripheral area. The sample still keeps its original shape and relatively dense structure, nearly no bone formation presents in its body, as shown in Figure 10 (D, G). However, the cement bodies of UFICPC3 (Figure 10E, H) and UFICPC7 (Figure 10F, I) become incomplete, and degraded area appears both on the outer surface and within their body, which is occupied by the NB (blue color). The formed bone network is mainly attributed to the fast degradation of ultrafine PCL fibers or

**Figure 10** 3D micro-CT reconstruction and 3D longitudinal section models before and after implantation.

**Notes:** 3D micro-CT reconstruction models of the reversed 3D porous structure without CPC matrix before implantation (A–C). UFICPC3 and UFICPC7 exhibited more and larger pore volume and interconnected channel-like pores throughout the shell and core. Also shown are 3D micro-CT reconstruction models of cements after implantation for 24 weeks (D–F) and 3D longitudinal section models of cements after implantation for 24 weeks (G–I). The pristine CPC degradation was slow and the bone regeneration was limited to the peripheral area (D, G). On the other hand, the cement bodies of UFICPC3 (E, H) and UFICPC7 (F, I) were fragmented, and the new bone (blue color) occupied both on the outer surface and within their body. Bar: 1 mm.

**Abbreviations:** CPC, calcium phosphate cement; CT, computed tomography; UFICPC, ultrafine fiber-incorporated CPC; 3D, three dimensional.
fiber bundles that leave behind abundant interconnected grooves and channels.

The fractions of BV/TV, MV/TV, and Tb. N from tomographic data of micro-CT are listed in Table 2. Compared to pristine CPC cement, the composites UFICPC3 and UFICPC7 cements showed higher BV/TV fraction and TV, as well as lower MV/TV fraction.

### Discussion

This work aimed to characterize the effect of the ultrafine PCL fibers on the in vitro and in vivo degradation as well as bone regeneration of CPC/PCL composites. Electrospun PCL fibers were collected by water pool and fabricated as bundles with nano to micro fibrous structure, as shown in Figure 2A. Two different weight percentages of ultrafine PCL fibers (3% and 7%) were incorporated into CPC matrix.

CPC is an osteoconductive and injectable material for filling of bone defects. However, the intrinsic porosity of pristine CPC after setting is too small for bone ingrowth. The introduction of macro- and microporosity within CPC can be used to promote CPC degradation and bone ingrowth. Therefore, two different strategies can be used to obtain porous CPC cements, i.e., the instantaneous or delayed approach. Instantaneous porous CPC involves the creation of CO$_2$ bubbles during setting, whereas delayed porous CPC is obtained by the incorporation of degradable polymeric microspheres or fibers into the CPC matrix. In the instantaneous foaming method, the pores created by upward migration of gas bubbles during setting cannot be controlled in terms of size and distribution. Incorporation of PLGA or gelatin microspheres in CPC cements results in the production of a controlled macro/microporosity during in situ degradation of the microspheres. However, the inclusion of PLGA microspheres is associated with a loss of mechanical strength of the set cement. Incorporated CPC with degradable fibers can be a major strategy to overcome the present limitations of CPC.

Absorbable fiber mesh, fiber mat, or suture fibers, like polyglactin 910, chitosan fiber, PLGA fibers, and Vicryl (a copolymer of glycolic acid and lactic acid), have been introduced into CPC cements to create macroporosity. However, a fiber content greater than 2–3 vol% results in poor workability and fiber dispersion of the cement paste. In view of this, electrospinning has been extensively explored as a method for the fabrication of nano- or micrometer fibers. Thinner diameter of fibers will provide a larger interface area between fibers and cement matrix for a given fiber volume fraction. As confirmed by our incubation assay, the subsequent porosity of CPC, which contains such ultrafine fibers, can indeed significantly be enhanced by the degradation of the incorporated fibers. After 7 days of incubation, a twofold macroporosity has been developed by the lipase catalyzed PCL degradation for UFICPC7 specimen, which was 24.5% vs the calculated fiber volume (12.29%). It can be also seen from the images in Figures 2C, D, 3E–L, and the reversed 3D porous structure in Figure 10B, C of composite cements that the interconnected fibrous structure have been formed in the fiber-incorporated cement matrix.

From a material point of view, PCL may not be a preferable degradable material like PLGA due to its long-term degradability. Despite this, electrospun fibers of PCL and PLGA have been visualized to have different morphologies. According to our previous study, ultrafine PCL fibers gathered as a bundle-like fibrilla but ultrafine PLGA fibers aggregated as a cotton-like material. The former is apparently easier to disperse into CPC matrix than the latter. In addition, a linear increase of weight loss with time has been found for both pure PCL fibers and the fiber composite cements (Figure 4), similar to the report of lipase catalyzed enzymatic degradation of PCL. Compared to PCL bulk, the degradability can be improved by increasing the interface of ultrafine PCL fibers. Fibrous PCL degrades through random hydrolytic chain scission of the ester linkage, which was confirmed by the decrease of the amorphous peak at 1,729 cm$^{-1}$ in the FTIR spectra (Figure 7). Thinner PCL fibers with a diameter from nano to micro scale become water-soluble and participate in the weight loss, larger body of this polymer require more scission steps to become degraded into sufficiently short fragments. This trend is nicely confirmed by monolayer degradation experiments. The incorporation and degradation of the ultrafine PCL fibers also apparently influenced the cement phase in vitro conversion. The weak acidic pH value, as caused by PCL degradation, can support the rapid hydrolytic conversion of monetite and α-TCP into HA phase (Figure 6), leading to a fast hardening of the CPC cement.

### Table 2 Bone (BV/TV), material (MV/TV) volume fraction, and trabecular number (Tb. N) calculated from micro-CT after 24 weeks of implantation

<table>
<thead>
<tr>
<th>Sample</th>
<th>24 weeks after implantation</th>
<th></th>
<th></th>
<th>Tb. N (1/mm)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>BV/TV (%)</td>
<td>MV/TV (%)</td>
<td></td>
<td></td>
</tr>
<tr>
<td>UFICPC0</td>
<td>6.31</td>
<td>84.39</td>
<td>2.03</td>
<td></td>
</tr>
<tr>
<td>UFICPC3</td>
<td>22.66</td>
<td>68.86</td>
<td>2.85</td>
<td></td>
</tr>
<tr>
<td>UFICPC7</td>
<td>23.66</td>
<td>67.05</td>
<td>3.34</td>
<td></td>
</tr>
</tbody>
</table>

**Note:** Both BV/TV fraction and trabecular number of UFICPC3 and UFICPC7 samples were higher than pristine CPC cement (UFICPC0).

**Abbreviations:** BV, bone volume; CPC, calcium phosphate cement; CT, computed tomography; MV, material volume; Tb. N, trabecular number; TV, tissue volume; UFICPC, ultrafine fiber-incorporated CPC.

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**International Journal of Nanomedicine 2016:11**

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The in vitro data and in vivo results confirmed that indeed the incorporation of electrospun PCL fibers promoted the degradation of the CPC cement and preliminary bone ingrowth. After in vitro immersion in lipase PBS, the grooves, and interconnected channels (Figure 3), the total porosity and macroporosity (Figure 5) dramatically increase with time in the ultrafine fiber-incorporated cement matrix. According to the data and images by micro-CT, the fraction of BV of sample UFICPC7 reaches 23.66% after 24 weeks of implantation (Table 2), and the degraded space has been occupied by a lot of newly formed bone (Figures 8–10). The fraction of BV of the two fiber-incorporated CPC composites (UFICPC3 and UFICPC7) was ~3.5 times higher than that of the pristine CPC (UFICPC0, only 6.31%).

Moreover, higher weight fraction of degradable fibers was more efficient in macropore formation and tissue infiltration. From longitudinal section of samples after 24-week implantation, more bone-like tissue (blue color) was observed inside the core of UFICPC7 sample (Figure 10I) than that of UFICPC3 (Figure 10H). The biological results in vivo matched the faster degradation (Figure 4) and higher macroporosity (Figure 5) in vitro. Both of them originated in higher fiber addition of UFICPC7.

Unfortunately, the degradation of PCL fiber in CPC matrix still caused some acidic problem in vivo even at pH value of 6.5, while testing for enzymatic degradation in vitro on day 7. Compared to UFICPC3, more inflammatory cells have been observed for more acidic products degraded from UFICPC7 samples (Figures 1B and 8). The amount of inflammatory cell infiltration and fibrous capsules have also been observed with the increasing implantation time. Normally, polycaprolactone is subjected to biodegradation as random hydrolytic chain scission of the ester linkage, and the products are either metabolized via the tricarboxylic acid cycle or eliminated by direct renal secretion.\(^{15}\) In this study, the acidic degradation products from PCL did not get completely neutralized by the soluble calcium ions of CPC according to our design. The hypothetic reason could be faster diffusion or concentration of acidic products. The former may be caused by more fiber dispersed in the surface of the UFICPC7 samples, and the latter always root from in situ degradation of thicker intertwined fibers (seen in the micro-CT cross sections). Thus, the degradation of fibers resulted in gathering of higher partial acidic products, which led to the acute inflammatory reaction and fibrous capsule hyperplasia, as shown in Figure 8. The same inherent cytotoxicity as potential inflammatory and foreign body reaction responses has also been discovered in similar types of systems as PLGA systems.\(^{20}\) Therefore, we should think about how to mix higher ratio of the ultrafine fibers or bundles into CPC cement to fabricate a homogenous composite, which could provide a more biofriendly environment and better interconnective porous structure for cells and tissue ingrowth in the next step.

It is noteworthy to mention that the ultrafine degradable fibers also assist the load of cytokines or drugs, by enabling a mild preparation process for drug delivery application.\(^{12}\) The functional fiber-incorporated cement composites would promote more efficient tissue regeneration and bone reconstruction in future.

**Conclusion**

Electrospun PCL fibers and fiber bundles have been incorporated into CPC matrix, and the effects of ultrafine PCL fibers on the degradability in vitro and in vivo were investigated. The incorporation of nano- to micrometer fibers significantly increased the macroporosity of cements and provided larger degraded space for bone formation and ingrowth than the pristine CPC cement. The in vitro and in vivo results demonstrate a promising method to use degradable ultrafine fibers in preparation of CPC bone cements or bone tissue engineering scaffolds.

**Acknowledgments**

The authors appreciate financial support from National 863 Project (No 2015AA033702), China NSFC project (31370971), and China-Netherlands PSA project (2008DFB50120 and PSA 08-PSA-M-02 [Dutch]).

**Disclosure**

The authors report no conflicts of interest in this work.

**References**


