A regenerative label-free fiber optic sensor using surface plasmon resonance for clinical diagnosis of fibrinogen

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Purpose: We present the regenerative label-free fiber optical biosensor that exploits surface plasmon resonance for quantitative detection of fibrinogen (Fbg) extracted from human blood plasma.

Materials and methods: The sensor head was made up of a multimode optical fiber with its polymer cladding replaced by metal composite of nanometer thickness made of silver, aluminum, and nickel. The Ni layer coated allowed a direct immobilization of histidine-tagged peptide (HP) on its metal surface without an additional cross-linker in between. On the coated HP layer, immunoglobulin G was then immobilized for specific capturing of Fbg.

Results: We demonstrated a real-time quantitative detection of Fbg concentrations with limit of detection of ~10 ng/mL. The fact that the HP layer could be removed by imidazole with acid also permitted us to demonstrate the regeneration of the outermost metal surface of the sensor head for the sensor reusability.

Conclusion: The sensor detection limit was estimated to be ~10 pM, which was believed to be sensitive enough for detecting Fbg during the clinical diagnosis of cardiovascular diseases, myocardial infarction, strokes, and Alzheimer’s diseases.

Keywords: SPR, real-time assay, histidine-tagged peptide, protein sensing

Introduction

In the past few decades, optical biosensors have been developed for applications in food industry, biomedical assay, and monitoring of environmental elements and changes.1–3 A great deal of effort has been made on developing various techniques for biomedical assays that use detection labels such as fluorophores to attach target molecules for specific4 and quantitative detection.5,6 However, it was known that a label-assisted assay revealed several drawbacks, such as an operation time that did not permit real-time assay, relatively high costs, and lack of reproducibility due to an inevitable assay dependence on operators.7,8 Alternatively, a label-free assay, which could replace a need of using such labels by utilizing the conversion of interaction of the target molecules with their sensor surface into a transducer signal, has been highlighted, and a variety of its detection platforms have been reported for the clinical diagnosis.9–12 Label-free biosensors that may support real-time assay could secure the specific detection of target molecules usually by resorting to their bio-affinity reactions or immunoreactions.5,13,14

One of the most widely used label-free bio-assays was optical biosensing with surface plasmon resonance (SPR), due to sufficiently high sensitivity and signal-to-noise ratio, and immunity to external electromagnetic disturbance. SPR

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is a resonant optical phenomenon occurring at an interface between a metal and a dielectric (eg, an aqueous medium), as a result of optical phase matching between evanescent waves of high propagation constant provided by attenuated total reflection (ATR), and nonradiative surface plasmon surface waves at the interface. This phase-matching condition, which governed the resonant coupling between those waves, can be altered sensitively with the refractive index of a dielectric in creating SPR occurrences at the interface with a metal. This resonant coupling condition could be served as a sensing principle for highly sensitive detection of concentration of target molecules in a quantitative and real-time manner. Recently, fiber optical SPR sensors have been demonstrated and brought considerable interest, owing to their miniaturized and simple structures, and their potential usability, as remote sensors with high sensitivity and wide dynamic range. However, a place where such remote sensors can be installed may not permit frequent replacement of sensor heads due to the limited accessibility, such as cosmic space, underground, and deserted lands with required sensor reusability.

Extensive researches have shown that human plasma fibrinogen (Fbg) could be considered one of the possible biomarkers for estimating risks of atherosclerosis, cardiovascular diseases, and Alzheimer's disease. It was also known that the elevated levels of plasma Fbg enabled the prediction of myocardial infarction and strokes. There were several methods to measure Fbg concentration, such as Clauss method, which relied on measuring thrombin clotting time for Fbg concentration. However, it was known that this method did not allow the quantification of Fbg concentrations in a real-time manner.

In this paper, we demonstrate a regenerative fiber optical SPR biosensor for immunoassay with its metal composite (Ag–Al–Ni) sensor surface for the quantitative real-time detection of Fbg concentrations. The heterogeneous metal layers were coated for high sensitivity, wide dynamic range of detection, and regeneration of the sensor surface. We immobilized a HP layer on the Ni surface for subsequent adsorption of Fbg antibody (immunoglobulin G [IgG]), which could capture Fbg molecules specifically. We monitored the successive adsorption of each layer of a HP, an IgG, and a human plasma-extracted Fbg in a real-time and quantitative manner. We also demonstrated that the sensor surface could eventually be regenerated (>95%) by removing the immobilized HP layer with IM and additional acetic acid (ACT). The regeneration of Ni surface demonstrated the enhanced capability of multiple measurements of target molecules on the same sensor head. This removes the need for replacement of a sensor head for another assay of different targets, and thus eliminates possibility of substantial change in light-coupling efficiency into the sensor head. The current regenerative SPR biosensor could find potential applications for use in places with limited accessibility for replacing sensor head.

**Materials and methods**

**Agents**

A HP (H$_2$N-HHHHHHGHHWGRGWVS-COOH) was synthesized by AnyGen Inc. (Kwangju, South Korea), while an IgG was purchased from EMD Millipore (Billerica, MA, USA). Histidine IM in HP could enable the coordinate metal bonding. Purified human Fbg was purchased from Sigma-Aldrich Co. (St Louis, MO, USA). Blocking buffer solution (B) was prepared for minimizing the nonspecific binding of injected Fbg to the HP layer, according to the block ace (AbDSerptec) instruction. All agents used were diluted with phosphate-buffered saline with Tween 20 (PBST; pH 7.4) obtained from Sigma-Aldrich Co.

**The SPR sensor head and sensing experimental setup**

A multimode optical fiber (JTFLH-Polymicro Technologies) with core diameter of ~200 μm was used to fabricate an SPR sensor head. A soldering machine was used to remove the polymer cladding of 5 cm length, and the subsequently exposed core surface was cleaned with solutions of ethanol and acetone for assuring the removal of remaining cladding substance. Using a thermal evaporator, the metal layers of ~36 nm thickness with Ag and ~4 nm thickness with Al were sequentially coated on the exposed fiber core for SPR excitation. Then, the radio-frequency magnetron sputter was used to deposit an Ni layer of 1 nm thickness, which should not significantly affect the SPR condition, determined by the coated Ag and Al.

A flow cell was made of polydimethylsiloxane in a circular shape with two ports for the inlet and outlet of flowing solutions. The heterogeneous metal-coated fiber was then installed into the flow cell.
Figure 1A shows the schematic of the experimental setup for label-free optical biosensing, based on output power measurement. He–Ne laser was used as light source at a wavelength of 632.8 nm. Laser light was coupled into the multimode optical fiber by an aspheric lens of a numerical aperture of 0.47 with its focus length of 4 mm. The acceptance angle of the fiber was ~21.72°. Light propagation through the clad-free fiber core of 5 cm length interfaced with coated layers of metals and supported multiple ATRs, and the injected solutions that flowed from an inlet to an outlet were expected to cause changes in output optical power, due to the SPR condition change. The fiber output light was collimated by an aspheric lens of a numerical aperture of 0.53. Use of a power meter connected to a computer enabled us to measure fiber output power and recorded corresponding power meter signals at a sampling rate of 20 Hz for a real-time monitoring.

Figure 1B and Figure 1C show that the metal coating was made in an asymmetrical manner by evaporating the metals on two opposite sides of an exposed fiber core. Thus, at least half the light that coupled into the fiber could be used for SPR excitation by using a circular polarization of input light theoretically, which could be prepared by placing a quarter-wave plate (λ/4) before the fiber. Decreased output power was observed as solution was injected into the flowing channel, due to enhanced ATR, which was governed by an SPR phase-matching condition, given by:

$$n_{\text{core}} \sin \theta_{\text{in}} = \text{Re} \left[ \frac{\varepsilon_{m} \varepsilon_{s}}{\sqrt{\varepsilon_{m}^{2} + \varepsilon_{s}^{2}}} \right]$$

(1)

where $n_{\text{core}}$ was the fiber core refractive index, and $\theta_{\text{in}}$ was the incidence angle of light at a boundary between fiber core and coated metal. $\varepsilon_{m}$ and $\varepsilon_{s}$ were relative permittivities of the metal composite and a dielectric (an aqueous medium to be sensed) on the outermost metal (Ni), respectively. The range of incidence angle at the core/cladding interface for total internal reflection was approximately 76°–90°. The immobilization of injected substance caused increases in $\varepsilon_{s}$ of the dielectric, leading to increased attenuation of reflected light off the fiber core. This resulted in a decrease in the fiber output power. It was known that the surface wave amplitude from the metal/dielectric interface decreased exponentially normal to the interface with a characteristic decay length $z$, as given by the following equation.

$$z = \lambda \left( \frac{\varepsilon_{m}^{2} + \varepsilon_{s}^{2}}{2 \pi \varepsilon_{s}} \right)^{1/2}$$

(2)
where $\lambda$ was the wavelength of light in vacuum, and $\varepsilon'_m$ was the real part of $\varepsilon_m$. For a dielectric value of a refractive index ranging from 1.33 (water) to 1.38 (bovine serum albumin), $z$ could be estimated as $\sim215.8–233.3$ nm, indicating the capability of detecting multilayers of bio/chemical molecules, including peptides and proteins on the metal.

**Results**

Figure 2 schematically illustrates the procedures for Fbg sensing, which cover from the sensor surface treatment to the surface regeneration. Firstly, the metal surface in the flow cell was cleaned by flowing PBST. Then, HP (1 $\mu$g/mL) was injected for immobilization on the Ni surface (1). The coordinate metal bonding of IM with Ni through nitrogen electrons enabled HP to be immobilized. We used Fbg antibody for stable bonding of Fbg with the surface, even in the presence of surface washout using PBST buffer. This IgG can also be used for selective bonding with Fbg in cases where various other kinds of proteins are present together, which was not our case. We injected Fbg antibody, IgG (0.375 $\mu$g/mL concentration, enzyme-linked immunosorbent assay dilution procedure 4,000 times) into the flow cell for IgG immobilization on HPs through peptide–peptide interaction (2).

To prevent the nonspecific binding of Fbg molecules to sites other than IgG, the sensor surface was passivated by B (0.4%, volume-to-volume ratio) (3) before immobilization of Fbg on the IgG (4). Note that injection of each layer of HP, IgG, B, and Fbg was followed by respective incubation of $\sim30$-minute duration. Again, a PBST solution was injected to wash away weakly bound molecules after each incubation. For the regeneration of the Ni surface, IM (20 mM) was injected to eliminate HP (5), and the final regeneration of the Ni surface (7) was performed with 1 M ACT and PBST (6).

The Ni surface regeneration could be checked by comparing the output power level of the fiber sensor between before (1) and after (6). In addition, the whole procedures (1)–(6) were repeated using the so-called regenerated Ni surface, to confirm the same (or similar) pattern of the sensor output signal in the repeats of identical procedures.

**Discussion**

Figure 3A shows the measured fiber output power in a real time, as a series of liquids of PBST, HP, IgG, B, four different concentrations of Fbg, IM, ACT, and PBST were injected successively. Injection of the series of liquids was followed by another set of injections of the same series of liquids as mentioned earlier. In both series of injected liquids, four different Fbg concentrations, that is, 10 ng/mL, 100 ng/mL, 500 ng/mL, and 1,000 ng/mL, were used. Each circular point

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**Figure 2** Procedures for regenerative sensing.

**Notes:** (1): HP immobilization; (2): association of IgG with HP; (3): passivation of surface with a blocking solution; (4): Fbg adsorption to IgG; (5): removing HP by imidazole; (6): removing imidazole by acetic acid and PBST; and (7): regenerated metal surface.

**Abbreviations:** HP, histidine-tagged peptide; IgG, immunoglobulin G (fibrinogen antibody); Fbg, fibrinogen; PBST, phosphate-buffered saline with Tween 20.
Figure 3 The sensor signals and the sensing surface regeneration.

Notes: (A) The SPR fiber sensor signals with a series of biochemical liquids injected for real-time label-free Fbg detection. Regeneration of metal (Ni) surface was achieved double times with the same fiber sensor. (B) AFM image for checking the metal (Ni) surface regeneration: (i) initial state, (ii) after immobilization of 1 μg/mL fibrinogen, (iii) after washing with imidazole, and (iv) after washing with ACT and PBST.

Abbreviations: PBST, phosphate-buffered saline with Tween 20; HP, histidine-tagged peptide (1 μg/mL); IgG, immunoglobulin G (fibrinogen antibody, 0.375 μg/mL); B, blocking buffer solution; Fbg, fibrinogen; IM, imidazole (20 mM); ACT, acetic acid; SPR, surface plasmon resonance; AFM, atomic force microscopy.
Table 1 Incubation time for HP, IgG, and Fbg

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<th>HP</th>
<th>IgG</th>
<th>Fbg</th>
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<tbody>
<tr>
<td></td>
<td>10 ng/mL</td>
<td>100 ng/mL</td>
<td>500 ng/mL</td>
</tr>
<tr>
<td>First series</td>
<td>40 minutes</td>
<td>30 minutes</td>
<td>35 minutes</td>
</tr>
<tr>
<td>Second series</td>
<td>40 minutes</td>
<td>30 minutes</td>
<td>30 minutes</td>
</tr>
</tbody>
</table>

Abbreviations: HP, histidine-tagged peptide; IgG, immunoglobulin G; Fbg, fibrinogen.

in Figure 3A represents the averaged value of sensor output power over 1 minute.

Note that Fbg of lower concentration was injected before injection of higher concentration, to clarify the signal change due to the lower concentration. The subsequent injection of higher concentration could lead to additional signal change. This led us to estimate that, for example, the total signal change induced by injection of 500 ng/mL Fbg should be the sum of those induced by 10 ng/mL, 100 ng/mL, and 500 ng/mL owing to the series of injection.

It was visible that injection of each liquid tended to cause rapid decreases in the sensor output, and the following incubation saturated the output to the stabilized one. The insets of Figure 3A display the stabilized sensor output (over ~15 minutes) for each Fbg concentration. The incubation time for a certain liquid immobilization could be defined as the time interval between the liquid injection and the start of the stabilized signal. The incubation time for HP, IgG, and Fbg from the measurement was estimated, as shown in Table 1.

As expected, larger changes in the sensor output power were observed from higher Fbg concentrations. Note that successive injections of IM, ACT, and PBST recovered the sensor output level nearly to that of the sensor output at initial state. Thus, the successive second regeneration of the sensor metal surface of the same fiber was demonstrated. This indicated that the layers of HP, IgG, and Fbg were physically removed successfully, since the fiber sensor was sensitive only to refractive indices of media on the sensor metal surface. Figure 3B shows atomic force microscopy images displaying physical regeneration of the Ni surface on the fiber sensor head, using IM, ACT, and PBST. It was also worth noting that the similar behavior of the observed sensor responses in the second series of liquid injection in comparison to the first series implied that the regenerated metal surface of the fiber sensor could support for a chemically reusable sensing platform, as well as physically reusable one.

The standard deviation of the sensor output power was measured (over 10 minutes time span) at the time just before the first Fbg was injected for each series of liquid injection. This meant that the standard deviation was obtained when PBST, HP, IgG, and B were present on the sensor metal surface. This standard deviation represented the sensor noise level (Δ), which was used to estimate its detection limit (S_{lim}).

\[
S_{lim} = (3A) \left( \frac{\partial C}{\partial P} \right)
\]  

where C was the concentration of Fbg, and P was the sensor output power level. The S_{lim} for the first-series injection was estimated to be approximately 3.40 ng/mL, corresponding to Fbg concentration of ~10 pM. S_{lim} for the second-series injection was 11.21 ng/mL (32.97 pM). This difference was associated with the incomplete regeneration of the sensor metal surface as shown in Table 2. We believe that the imperfection of regeneration resulted from incomplete removal of HP and remaining plasma proteins adsorbed nonspecifically on it. In addition, there is a possibility that the used acid may change the metal surface state. This may have reduced its detection limit in the second series of liquid injection. The sensor platform presented allowed the detection limits which were comparable to a conventional enzyme-linked immunosorbent assay method or a typical SPR sensor system based on the prism-coupled Kretschman–Raether configuration. The estimated detection limits were believed to be lower than that required for diagnosis of the aforementioned diseases. Moreover, these detection limits for specific detection of Fbg were lower than that using Raman spectroscopy or comparable to those reported using local SPR excited by nanoparticles.

Figure 4 shows the differential changes in the sensor output power as a function of Fbg concentration by averaging measured data obtained with all Fbg concentrations of both series of liquid injections. Note that nonzero four concentrations of 10 ng/mL, 100 ng/mL, 500 ng/mL, and 1,000 ng/mL were used in a row. This means that the

Table 2 Regeneration degree of the sensor surface for both series of liquid injection

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<thead>
<tr>
<th></th>
<th>After IM washing</th>
<th>After washing with ACT and PBST</th>
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<tr>
<td>First series</td>
<td>76.83%</td>
<td>97.85%</td>
</tr>
<tr>
<td>Second series</td>
<td>72.82%</td>
<td>97.05%</td>
</tr>
</tbody>
</table>

Abbreviations: IM, imidazole; ACT, acetic acid; PBST, phosphate-buffered saline with Tween 20.
ultimate concentrations that caused signal to change from that immediately before the first concentration injection must be reestimated as accumulated ones, that is, 10 ng/mL, 110 ng/mL, 610 ng/mL, and 1,610 ng/mL. In this regard, the concentration range of Fbg detected was ~1,610 ng/mL.

Note that the concentration range of Fbg relied not only on detection device characteristics but also on the concentration of Fbg antibody (IgG) immobilized on the sensing surface. It is generally seen that the more the concentration of IgG immobilized is, the wider the concentration range of Fbg detected is.

Higher concentrations produced larger changes in the output power in an approximately linear fashion. However, the plot showed nonlinear behavior at around the lowest concentration (10 ng/mL), accounting for the steeper slope of the sensor signal change with respect to the Fbg concentration change. This is due to the fact that higher intensity of SPR wave was present at region closer to the metal surface. This led to stronger coupling between SPR wave and the Fbg molecules.

The use of HP for antibody immobilization onto Ni surface could offer several benefits to the sensing surface treatment for a label-free optical immunoassay, as described in the following. First, the use of HP could allow simultaneous removal of a pair of a target protein and its antibody, leading to the regeneration of the sensor metal surface. As described earlier, IM with ACT and buffer solution (PBST in this work) could efficiently eliminate HP, the antibody IgG, and Fbg (target protein) in recovering Ni surface for sensor reusability. As shown in Figure 5, nitrogen (N), the electron donor of the IM ring of histidine molecules, formed the coordinate metal bonds with Ni. A carboxyl acid group of the peptide side of HP was responsible for its bonding with an antibody IgG. For the regeneration of Ni surface, we injected IM (20 mM with 10-minute incubation) to break HP bonds with Ni. This enabled subsequent elimination of IM molecules away from the Ni surface, and therefore, a pair of IgG and Fbg would be washed away from the sensor surface by flowing ACT and PBST. Secondly, HP could be used to immobilize different kinds of antibodies through engineering of its constituent peptides, thus supporting its applicability to various proteins sensing in a label-free biosensor. Lastly, the use of HP could enable one to avoid

Figure 4 Differential change in the sensor output power with increasing concentration of fibrinogen.

Notes: \( \Delta P \) denotes the change in sensor output power, and \( C \) is the Fbg concentration accumulated on the sensor surface in a series injection of different Fbg concentrations.

Figure 5 Immobilization of HP on the Ni surface.

Abbreviation: HP, histidine-tagged peptide.
denaturalization of a sensor metal surface, which may be encountered when whole metal surface was treated with toxic chemical cross-linker.  

Table 2 illustrates the degrees of regeneration of the metal surface, which represents how close was the signal (sensor output power) recovered from binding of the last Fbg concentrations toward the original (start) signal (before HP injection), as a result of injection of IM, ACT, and PBST. In the first series of liquid injection, ~77% signal recovery was achieved by IM injection, and eventually ~98% recovery by additional washing with ACT and PBST. Similarly, in the second series of liquid injection, IM injection produced 73% signal recovery with subsequent signal recovery of 97% by additional ACT and PBST. This meant that the regeneration of Ni surface could be fulfilled multiple times for the sensor reusability. The procedures required for the metal surface regeneration turned out to be relatively simple compared to those using toxic chemical treatment which could damage and denature the sensor metal surface, such as piranha solution and sodium hypochlorite solution methods.

Conclusion
A label-free regenerative immuno-biosensor was demonstrated with a sensor key head, which comprises a multimode optical fiber with SPR coating for detecting Fbg of various concentrations quantitatively in a real-time manner. The key ingredient for regeneration procedure of immuno-assay was the immobilized HP layer on the sensor metal surface. This HP layer for binding IgG was able to be eliminated from the metal surface by using IM, ACT, and PBST for such regeneration.

The regeneration was demonstrated twice (using two identical series of liquid injection), to check its chemical validity, as well as the physical one. The regeneration of the sensor metal surface could open potential applications for biosensors in needs for limited human access, such as cosmic space, underground, and deserted lands. The detection limit of the sensor was estimated to be ~3.40 ng/mL (10 pM) and 11.21 ng/mL (32.97 pM) in the first and second series of liquid injection, respectively. The label-free detection platform may find potential applications for Fbg-based diagnosis of cardiovascular disease, strokes, heart disease, and Alzheimer’s disease.

Actual application of this sensor device in the practical use would require calibration of the sensor signal in diagnosing different concentrations of injected Fbg. However, one must note that this calibration would depend on IgG concentrations and metal coating thickness, which would determine the SPR wave decaying depth normal to the metal surface.

The presented sensing scheme in using a multimode optical fiber used neither any spectroscopic technique nor measurement of incident angle of an optical beam, unlike conventional SPR biosensor, but the present sensor would be miniaturized easily and integrated into a lab-on-chip platform.

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Disclosure
The authors report no conflicts of interest in this work.

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