The mechanical and biological studies of calcium phosphate cement-fibrin glue for bone reconstruction of rabbit femoral defects

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Abstract: In order to improve the mechanical and biological properties of calcium phosphate cement (CPC, nanometer-biomaterial) for bone reconstruction in the rabbit femoral defect model, fibrin glue (FG, the natural product, purified from the blood) was introduced at three different ratios. The CPC powder and the FG solution were mixed, respectively, at the powder/liquid (P/L) ratios (g/mL) of 1:1, 3:1, and 5:1 (g/mL), and pure CPC was used as a control. After being implanted into the femoral defect in rabbit, the healing process was evaluated by micro-computed tomography scan, biomechanical testing, and histological examination. By micro-computed tomography analysis, the P/L ratio of 1:1 (g/mL) group indicated the largest quantity of new bone formation at 4 weeks, 8 weeks, and 12 weeks after implantation, respectively. Bone volume per trabecular volume of the 1:1 group was highest in the four groups, which was 1.45% ± 0.42%, 7.35% ± 1.45%, and 29.10% ± 1.67% at 4 weeks, 8 weeks, and 12 weeks after the operation, respectively. In the biomechanical tests, the compressive strength and the elastic modulus of the three CPC–FG groups were much higher than those of the pure CPC group at the determined time point (P < 0.05). The histological evaluation also showed the best osseointegration in the 1:1 group at 4 weeks, 8 weeks, and 12 weeks after the operation, respectively. In the 1:1 group, the bone grew into the pore of the cement in the laminar arrangement and connected with the cement tightly at the 12th week after the operation. This present study indicated that the CPC–FG composite at the P/L ratio of 1:1 (g/mL) stimulated bone regeneration better than any other designed group, which suggested that CPC–FG at the P/L ratio of 1:1 has significant potential as the bioactive material for the treatment of bone defects.

Keywords: calcium phosphate cements, fibrin glue, bone reconstruction, micro-CT, biomechanical testing, histological examination

Introduction

The reconstruction of segmental bone defects, which are caused by trauma, cancer, and metabolic disorders, remains the major challenge in orthopedics. Although autogenous bone grafts are still regarded as the golden standard for the treatment of bone defects, insufficient availability of grafting tissues and postoperative donor-site morbidity limit the application of bone autografting.1–3 Furthermore, the application of bone allograft is also restricted by its antigenicity and the risk of disease transmission.4 As a result, it is required to produce the ideal materials that could overcome the disadvantages of the grafting tissues.

Synthetic material is the promising bone substitute, which could offer unlimited availability without causing donor-site morbidity and disease transmission. Calcium phosphate, such as hydroxyapatite (HA), β-tricalcium phosphate, and calcium...
phosphate cements (CPC) are well researched, widely used, and have been proven to have good biocompatibility and bioactivity.\textsuperscript{5-7} Moreover, they are all resorbable and non-inflammatory, without causing immunological responses and having excellent osteoconductive ability. Nevertheless, both HA and \( \beta \)-tricalcium phosphate are solid and prefabricated materials with a certain shape, which need to be remodeled to fit the shape of the defect in the clinic.\textsuperscript{8}

In contrast, CPC is a mixture at certain determined powder to liquid (P/L) ratios and can form the remodeled and injectable paste, which facilitates the operative procedure and fills the irregular bone defect easily. CPC was firstly reported by Chow and Brown.\textsuperscript{9} Since then, CPC has been investigated by many material scientists, and the first marketed product (BoneSource\textsuperscript{9}, Stryker Instruments, Kalamazoo, MI, USA) was developed in the 1990s. Nowadays, a number of types of CPCs are commercially available, and most of them are the nanometer product. In addition to the commonness of the calcium phosphate materials, CPC has two main advantages. Firstly, CPC is obtained by mixing one or several reactive calcium phosphate powders with an aqueous solution to form the solid calcium phosphate at room temperature. Secondly, this cement could be easily shaped to fill irregular bone defects and cavities. However, it still has some disadvantages, especially with respect to its mechanical properties. CPC is the brittle ceramic and the 0.2\% deformation strain could cause shape failure.\textsuperscript{10} It is desirable to increase the mechanical properties of CPC and therefore make it bear larger deformation strains.

In order to improve the mechanical properties of CPC, other injectable materials such as chitosan, gelatin, and collagen have been introduced into this material.\textsuperscript{11,12} Fibrin glue (FG) is a kind of elastomeric, biocompatible material with sufficient adhesive strength, which has been approved by the Chinese State Food and Drug Administration. Because of its adhesive properties, hemostatic activity, and wound healing process, this biological adhesive is widely used in surgery for repairing tissue damage and blood vessel injury. Some material scientists found that FG could stimulate bone formation in a mouse study.\textsuperscript{13} In a previous study, FG-coated calcium phosphate and glass ceramics were implanted into the extraskeletal site of male Swiss albino mice. The new bone formation was observed in the FG-coated groups. Some additional studies supported the standpoint that the FG stimulates bone formation.\textsuperscript{14,15} Different sizes and different ratios of composites always have different properties;\textsuperscript{16} it is unclear whether a different ratio of CPC and FG has different properties for bone reconstruction.

In this study, we prepared the injectable composites by mixing CPC and FG at different P/L ratios and investigated the optimal P/L ratio between CPC and FG for repairing bone defects in vivo. We hypothesized that: (1) CPC powder and FG, mixed at the optimal ratio, could realize a good match between material degradation and new bone formation; and (2) the introduction of FG could improve the mechanical properties of CPC and improve osteoconduction for new bone formation.

**Materials and methods**

**Preparation of CPC–FG composites**

The CPC powder (the nanometer product; Shanghai Rebone Biomaterials Co, Ltd, Shanghai, People’s Republic of China) and FG (Guangzhou Bioseal Biotech Co, Ltd, Guangzhou, People’s Republic of China) used in this study were approved by the Chinese State Food and Drug Administration. Firstly, the CPC powder and FG solution were mixed at different P/L ratios (g/mL): 5:1, 3:1, and 1:1 in sterile injection syringes. The mixture was then injected into a 6 mm (diameter) \( \times \) 10 mm (height) cylinder mould. After being set in a humidor with 100\% relative humidity at 37\( ^\circ \)C for 4 hours, the specimen was remolded. The same CPC powder mixed with water at the P/L ratio of 3:1 (g/mL) was also prepared as a control. For the in vivo studies, the specimens were prepared under aseptic conditions 1 day before operations.

**SEM observation**

The composites were freeze-dried and coated with gold, and they were then examined under a 20 kV scanning electron microscope (SEM; S-3000N; Hitachi, Ltd, Tokyo, Japan).

**Surgical procedure**

Sixty adult (1–1.5 years) male New Zealand White rabbits (provided by the Experimental Animal Center of the Fourth Military Medical University, Xi’an, Shaan, People’s Republic of China), weighing from 2.8 kg to 3.5 kg (average weight, 3.0 kg), were used in the study. The animal experiments were performed according to the protocols approved by the Institutional Animal Care Committee of the Fourth Military Medical University (permit number: 12014). At first, all the animals were randomly divided into four groups and each group had 15 animals. General anesthesia was induced by intramuscular injection of ketamine hydrochloride at a dose of 35 mg/kg. All the rabbits were fastened onto a special plate in prone position to avoid any movement of their body during the operation. After shaving and disinfecting, the lateral longitudinal incision was performed in the bilateral femoral.
condyles of each animal. A cavity-like defect (diameter: 6 mm, depth: 10 mm) was made by a drill under abundant saline irrigation to avoid necrosis. The CPC–FG composite was implanted into the cavity of each rabbit from the four groups. After implantation, the operative area was rinsed with saline and the incision was closed in layers. After the operation, the rabbits were treated with penicillin (240,000 UI) for 3 days postoperatively.

Five animals from each group were sacrificed using an overdose of sodium pentobarbital at 4 weeks, 8 weeks, and 12 weeks after the operation. The material and surrounding bone tissue of the femoral condyles of each animal were harvested. The left femurs of each animal were used for biomechanical tests and were stored at −20°C until use. The right femurs were used for micro-computed tomography (CT), and histological examinations were fixed in formaldehyde (10%) for 3–5 days before application.

**Biomechanical testing**

The mechanical tests were performed after the soft tissue of the femoral condyles was removed. Every specimen was shaped into the 6 mm (diameter) × 10 mm (height) cylinder by a tubular drill (6 mm in diameter). Five specimens were tested from every group at 4 weeks, 8 weeks, and 12 weeks after implantation. The specimens without operation were tested at 0 weeks. Their diameters and lengths were precisely measured and recorded. The specimens were composed of the newly formed bone tissue and the residual materials. The mechanical properties of the specimens were analyzed by a materials testing machine (MTS-858; MTS Systems Corporation, Eden Prairie, MN, USA). An unconfined compression test was performed on hydrated scaffold samples at a deformation rate of 5 mm/minute until failure. We calculated the data with the following formulas:

\[
\text{Compressive strength (MPa)} = \frac{\text{Failure load}}{\text{compression area}} \tag{1}
\]

\[
\text{Elastic modulus (GPa)} = \frac{\text{Stress}}{\text{deformation}} \tag{2}
\]

**Micro-CT analysis**

The specimens (n = 5) were examined by a micro-CT (eXplore Locus SP Pre-Clinical Specimen MicroCT; GE Healthcare Bio-Sciences Corp, Piscataway, NJ, USA) operated at a 14 µm isotropic resolution to evaluate the new bone formation and the degradation of the materials. The threshold algorithm provided by the manufacturer of the micro-CT unit was applied to separate bone tissues from nonbony tissues. The implanted cylinder, with a diameter of 6 mm and a height of 10 mm, was chosen as the region of interest (ROI). The scanned slices were reconstructed in high solution to show the new bone formation and the degradation of the implants due to the different threshold for the bone and the material, which were analyzed by Microview software (GE Healthcare Bio-Sciences Corp). The residual material volume of residual fraction (RMVF) was calculated as the ratio between the volume of the residual material and the total volume of the materials within the ROI in each defect site, which could evaluate the degradation rate of the material. RMVF = bone volume per trabecular volume (VV/TV), in which VV is the volume of the residual material and TV is the total volume of the material. BV/TV was calculated, and the amount of the new bone formation into the cement was defined as the ROI, in which BV is the volume of the new bone formation and TV is the total volume of the implantation.

**Histological examination**

Following micro-CT scan, the specimens were dehydrated through a series of graded ethanol (70%–100%). Then, the bones were subsequently cleared in toluene and embedded in methylmethacrylate without decalcification. Cross-sections with a thickness of approximately 200 µm were cut from each specimen by a hard tissue microtome (Reichert-Jung Leica SP1600; Leica Microsystems, Wetzlar, Germany). Thereafter, the sections were polished into a thickness of 50–60 µm with an Exakt Grinder (EXAKT Advanced Technologies GmbH, Norderstedt, Germany). Finally, the slides were glued onto a plastic support, and stained with Van Geison stain for histological examination.

**Statistical analysis**

Statistical analysis was performed using the Statistical Package for the Social Sciences statistical software (SPSS, version 13.0; SPSS, Inc, Chicago, IL, USA). The data was presented as the mean ± standard deviation, and levels were compared by a one-way analysis of variance and Student’s t-test. P-values less than 0.05 were considered significant.

**Results**

**SEM observation**

Figure 1 displayed the images of the different P/L ratios of CPC–FG and pure CPC samples, which were observed by SEM. The differences in the surface morphology of CPC and FG behaved differently. FG presented with a relatively denser and smoother structure compared with CPC. In the pure CPC group, the morphology of a rough surface on the
samples was always evident. As the FG content increased from a 5:1 P/L ratio to a 1:1 P/L ratio, the samples showed more contact between the CPC particles and the gel FG, and the round pores of the cements became smaller and closer.

Biomechanical testing
The results of the compressive strength were plotted in Figure 2 (n = 5). The compressive strength of each CPC–FG group was much higher than that of the pure CPC group, whatever the implantation period (P < 0.05). Compressive strength of the pure CPC decreased after implantation from week 4 to week 12. The compressive strength of the pure CPC at the different implantation periods of 4 weeks, 8 weeks, and 12 weeks remained lower than the data observed before implantation. However, the compressive strength of the three ratios of CPC–FG all increased at week 4 after the operation, and decreased from week 8 to week 12. The compressive strength of CPC–FG at the P/L ratio of 5:1 (g/mL) was highest at any determined time in the four groups.

Figure 2 also shows the results of the elastic modulus studies. The elastic modulus of the CPC group was much lower than that of any CPC–FG group at each time point (P < 0.05). The results of the CPC–FG groups at ratios of 1:1, 3:1, and 5:1 all increased at 4 weeks after implantation, and decreased at 8 weeks and 12 weeks after implantation.

Micro-CT analysis
After 4 weeks, the newly formed bone showed little direct contact with the cement in all the four groups. The 1:1 group showed a slightly greater amount of newly formed bone in the peripheral portion of the cement than any other group (Figure 3). Eight weeks later, the zone in which the bone made contact with the cement increased due to the new bone formation. At the same time, the cylinder of cement had been partly absorbed and replaced by newly formed bone trabeculae in the periphery. The 1:1 group showed the largest new bone formation at both the peripheral and central areas of the cement (Figure 4). After 12 weeks, the degradation of the materials continued, and the bone regeneration continued at the same time. The 1:1 group also showed the fastest degradation of the material and the best new bone formation in the four groups (Figure 5). The data in Figure 6 supported the images observed during micro-CT. The RMVF of the 1:1 group was lowest at any determined time.
after the operation, which was 87.01% ± 1.96% at 4 weeks, 76.90% ± 2.34% at 8 weeks, and 63.21% ± 2.89% at 12 weeks, respectively. The BV/TV of 1:1 group was the highest in the four groups, which was 1.45% ± 0.42%, 7.35% ± 1.45%, and 29.10% ± 1.67% at 4 weeks, 8 weeks, and 12 weeks after the operation, respectively.

**Histological examination**

The bone, cartilage, fibrous tissue, and residual material were stained into red, purple, blue, and black colors, respectively, by Van Geison staining. After 4 weeks of implantation, the bone growth in the composite was hardly observed in all groups. In the 1:1 group, the peripheral layer around the material had stained purple, where the new bone growth was apparent in the cartilage. In the 3:1 group, the cartilage could also be observed, which was not as evident as it was in the 1:1 group. There was no obvious indication of osteogenesis in the 5:1 group and the CPC group (Figure 7).

With the increase of the implantation period of up to 8 weeks, the bone was deposited directly onto the implant surface and connected tightly in both the 1:1 and 3:1 groups. In the 5:1 group and the CPC group, the conjunction between the bone tissue and the cement was not as tight as that in the 1:1 group and the 3:1 group (Figure 8).

Further increasing the implantation period to 12 weeks, the bone in the 1:1 group grew into the pore of cement and appeared to be in the laminar arrangement. The material showed a good osseointegration effect with the bone tissue. In contrast, in the 3:1, 5:1, and CPC groups, the interface between the bone and materials were not as tight as observed in the 1:1 group, and the implanted cement was not as obviously substituted by bone tissue as was found in the 1:1 group (Figure 9). Inflammatory cells or acute inflammation processes were not observed in any of the groups.
Discussion

In this study, three different ratios of CPC–FG and pure CPC were investigated histologically and biomechanically after they were implanted in rabbit femoral defects. The CPC–FG group at the ratio of 1:1 (g/mL) exhibited the best bone formation and interface conjunction in the micro-CT analysis and histological analysis at 4 weeks, 8 weeks, and 12 weeks after implantation in the four groups. The compressive strength and the elastic modulus of each CPC–FG group were both higher than those of the pure CPC group, whatever the implantation period ($P < 0.05$).

Nowadays, CPC is the good osteoinductive and osteoconductive material known by material scientists and is widely used in bone tissue engineering. However, the poor mechanical property of CPC has limited its application into the nonload-bearing condition.17,18 From this biomechanical testing in vivo, it is easy to find that the compressive strength and the elastic modulus of each CPC–FG group was higher than those of the pure CPC group, whatever the implantation period. It seemed that FG effectively enhanced the mechanical properties of CPC. The incorporation of polymers into CPC has been a well known strategy over the mechanical limitations. By adding polymers including gelatin, chitosan, and collagen in either the powder phase or the liquid phase, the mechanical property, biocompatibility, and bioactivity of CPC all improved.19–21 In this study, the pure CPC relied solely on the apatite crystals in order to interlock to provide strength. FG was well distributed in the CPC–FG composite by the SEM observation of this study. The CPC–FG composites not only had interlocking crystals, but it also had additional FG, which could bind the apatite crystals together. Some material scientists also reported that porosity, pore size, and pore size distribution increased by adding higher volumes of FG into CPC.22 The porosity, pore size, and pore size distribution could affect the biomechanical properties of the materials. This could be the reason why the compressive strength of the 5:1 group was the highest in the four groups. Some material scientists reported that the CPC–FG composite showed signs of transformation and growth of the crystalline phase of the CPC particles after being immersed in Ringer’s solution for 3 days, due to the polymerization of fibrinogen and thrombin.22 As the interfacial bonding between CPC and FG increased, the compressive strength and the elastic modulus of each CPC–FG group increased in the early stage in vivo. Owing to the degradation of FG in vivo, the mechanical properties decreased at a later stage. It was concluded that the cross-linking of CPC and FG, the degradation of the material, and the maturation of the bone together resulted in this dynamic tendency.

Previous research has shown that CPC performed the different tissue reactions in cortical bone, cancellous bone, and medullar bone;23 the best bone regeneration was observed in cortical bone, the medullar bone was the worst. The material biodegradation was the highest in the medullar bone, and the cortical bone was the lowest. To evaluate the functionality of the biomaterial, the cancellous bone is the suitable site.23 Some researchers reported that the compressive strength of the cancellous bone is about 3.75 MPa, and the elastic modulus of the cancellous bone is about 1.75 GPa.24 In this study, the compressive strength and the elastic modulus of the CPC–FG specimens at the P/L ratio of 1:1 (g/mL) were the closest to those of cancellous bone in the four groups. In this study, the surgical area was the femoral condyle of the rabbit, and the implanted material was surrounded by the cancellous bone in vivo. The hypothesis was that the CPC–FG cement at
the ratio of 1:1 (g/mL) had similar mechanical properties as the surrounding bone. In this system, the surrounding bone could get adequate mechanical stimulation, which could induce new bone formation.

The results in this study demonstrated not only good mechanical compatibility, but also good biocompatibility of CPC–FG at the P/L ratio of 1:1 (g/mL). The micro-CT analysis and the histological analysis both showed that the CPC–FG at the P/L ratio of 1:1 (g/mL) resulted in better bone formation and interface conjunction than any other group. It was considered that the pore size of the cement could be one reason for this result. CPC is a family of materials that includes self-setting HA and brushite, which is the main component in bone matrix, and which is obtained by soft chemistry routes. CPC powders are intrinsically porous materials. Moreover, CPC possesses micro- or nanometer range pores, but it lacks macropores, which are essential structures for tissue colonization. The bone tissue grows on the surface of CPC and is unable to penetrate inside the material due to the small size of the pores.

CPC has a low degradation rate, which remained more than 78 weeks after being implanted into the dog femur. Some scientists also reported that the degradation rate of the FG is approximately 10–14 days. The degradation rate of the CPC–FG should be in line with the degradation rate of FG. FG in CPC–FG degraded in vivo, which was helpful for the material to form the macroporous structure. FG has been used as a hemostatic agent and a sealant for decades. It has two components: fibrinogen and thrombin. When the two components are mixed, the thrombin activates the fibrinogen to form the fibrin clot. In this study, three P/L ratios of CPC–FG equaled three different ratios of thrombin concentrations and three different ratios of ionic strength of the solution. Some researchers reported that the cement pore size and the fiber diameter were dependent on cross-linking time, which changed in accordance with the thrombin concentration or the ionic strength of the solution. The pore size and the fiber diameter affected both the structure and degradation of the gel. The degradation of the material and the regeneration of new bone could have the dynamic balance to make the optimal bone regeneration. From the micro-CT analysis (Figure 5), it was easily found that the degradation of the material was earlier than the regeneration of the new bone. It indirectly demonstrated that the degradation of the material changed the pore size of the implanted cement, which affected new bone regeneration. It was possible that CPC–FG at the P/L ratio of 1:1 (g/mL) may form the pore size suitable to achieve a dynamic balance for cement degradation and the bone regeneration.

CPC is a kind of material that has good biocompatibility; however, it generally has low cell attachment and low proliferation rates in cell cultures in vitro. Our previous in vitro study demonstrated that the CPC–FG scaffold could support bone marrow stromal cell attachment and proliferation, equal to that of the CPC control, and no obvious difference existed between CPC–FG and pure CPC; however, in this in vivo study, a different situation was shown. The CPC–FG composite had a better effect on bone formation than the CPC control. It was possible that the environment of the cell was also a problem. The cell culture was a closed and static system in vitro, which was different from the study in vivo. Several researchers reported that FG was a reservoir for several growth factors during the in vivo degradation, such as for vascular endothelial growth factor, basic fibroblastic growth factor, transforming growth factor-B1, and growth factor-binding proteins such as insulin-like growth factor-binding protein-3 for insulin-like growth factor. These factors could change the cell culture in vivo.

**Conclusion**

The introduction of FG into CPC can improve the mechanical strength and osteoinductivity of CPC. The in vivo experiments indicated that the CPC–FG composition at the P/L ratio of 1:1 showed the best effects for enhancing new bone formation and for improving the mechanical properties of the operation areas. The findings may help surgeons find a good additive and an optimal P/L ratio in the application of CPC. Further studies are necessary to investigate the mechanism of osteogenesis induced by the CPC–FG composite. First, the in vivo osteoinductive effect of the FG in the CPC needs to be clarified. Second, CPC–FG directly injected into the defect should be added to compare osteogenesis when it was implanted into the defect. And third, mechanical properties of CPC–FG need to be studied to find its relationship with new bone formation.

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**Disclosure**

The authors report no conflicts of interest in this work.

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